

Set 1 of CERES Data Products

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Wielicki et al. (1996) (BAMS): Clouds and the Earth's Radiant Energy System (CERES)

"Obtaining surface fluxes from measured TOA fluxes, CERES investigations are examining two independent approaches"

Approach 1. Establishing direct relationships between TOA radiative fluxes and surface fluxes.

Approach 2. Surface fluxes can be calculated by radiative transfer computations.

CERES ATBD (Algorithm Theoretical Basis Document) (Wielicki and Barkstrom 1996):

“CERES will provide two types of surface fluxes: *first*, a set which attempts to directly relate CERES TOA fluxes to surface fluxes; *second*, a set which uses observed properties to calculate surface, in-atmosphere and TOA radiative fluxes by radiative transfer model”. (Emphasis in the original)

Set 2 has been successfully generated by the Surface-Atmosphere Radiation Budget (SARB) Working Group.

Set 1 seems to be abandoned. Since no Direct TOA-Surface Relationships (DTSR) Working Group was established, I did the job.

Wielicki et al. (1996) refer to Li et al. (1993a) for SW, and for LW to **Inamdar and Ramanathan (1995)** and **Stephens et al. (1994)**.

Observations of the Earth's Radiation Budget in relation to atmospheric hydrology

4. Atmospheric column radiative cooling over the world's oceans

Graeme L. Stephens,¹ Anthony Slingo,² Mark J. Webb,² Peter J. Minnett,³
Peter H. Daum,³ Lawrence Kleinman,³ Ian Wittmeyer,¹ and David A.
Randall¹

(Section 4)

4. Flux Ratios and a Simple Description of the Planetary Greenhouse Effect

$$\mu \frac{dI(\tau, \mu)}{d\tau} = I(\tau, \mu) - B(T) \quad (1a)$$

$$-\mu \frac{dI(\tau, -\mu)}{d\tau} = I(\tau, -\mu) - B(T), \quad (1b)$$

for upward (F^\uparrow) and downward (F^\downarrow) hemispheric fluxes
leads to

$$\frac{dF^\uparrow}{d\tilde{\tau}} = F^\uparrow - \pi B, \quad (3a)$$

$$-\frac{dF^\downarrow}{d\tilde{\tau}} = F^\downarrow - \pi B, \quad (3b)$$

The solution for upward (F^\uparrow) and downward (F^\downarrow) fluxes:

$$\sigma T_s^4 = \frac{F_\infty}{2} [2 + \tilde{\tau}_s] \quad (5a)$$

$$F_g = F^\downarrow(\tilde{\tau}_s) = \frac{F_\infty}{2} \tilde{\tau}_s \quad (5b)$$

Observations of the Earth's Radiation Budget in relation to atmospheric hydrology

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$$F_g = F^\downarrow(\tilde{\tau}_s) = \frac{F_\infty}{2} \tilde{\tau}_s \quad (5b)$$

With

$$F_0(\tau_s) = \sigma T_0^4 = \frac{F_\infty}{2} (1 + \tau_s)$$

which is Eq. (2) in Stephens et al. (1991),
they are equivalent to the three terms in
Schwarzschild's two-stream (1906, Eq. 11):

$$E = \frac{A_0}{2} (1 + \bar{\tau}), \quad A = \frac{A_0}{2} (2 + \bar{\tau}), \quad B = \frac{A_0}{2} \bar{\tau}.$$

These are TOA-surface flux ratios, but not *direct*,
since they depend on atmospheric properties via τ .

But the difference of the middle and the first term
is really direct:

$$A - E = \frac{A_0}{2} \Leftrightarrow$$

$$\sigma T_s^4 - \sigma T_0^4 = \frac{F_\infty}{2}$$

Eq. (1) of Set 1

Graeme L. Stephens: Radiative Transfer Notes AT 622

Colorado State University (1992-2013)

https://reef.atmos.colostate.edu/~odell/AT622/stephens_notes/AT622_section06.pdf

Example 6.3: Skin temperatures and temperature discontinuities

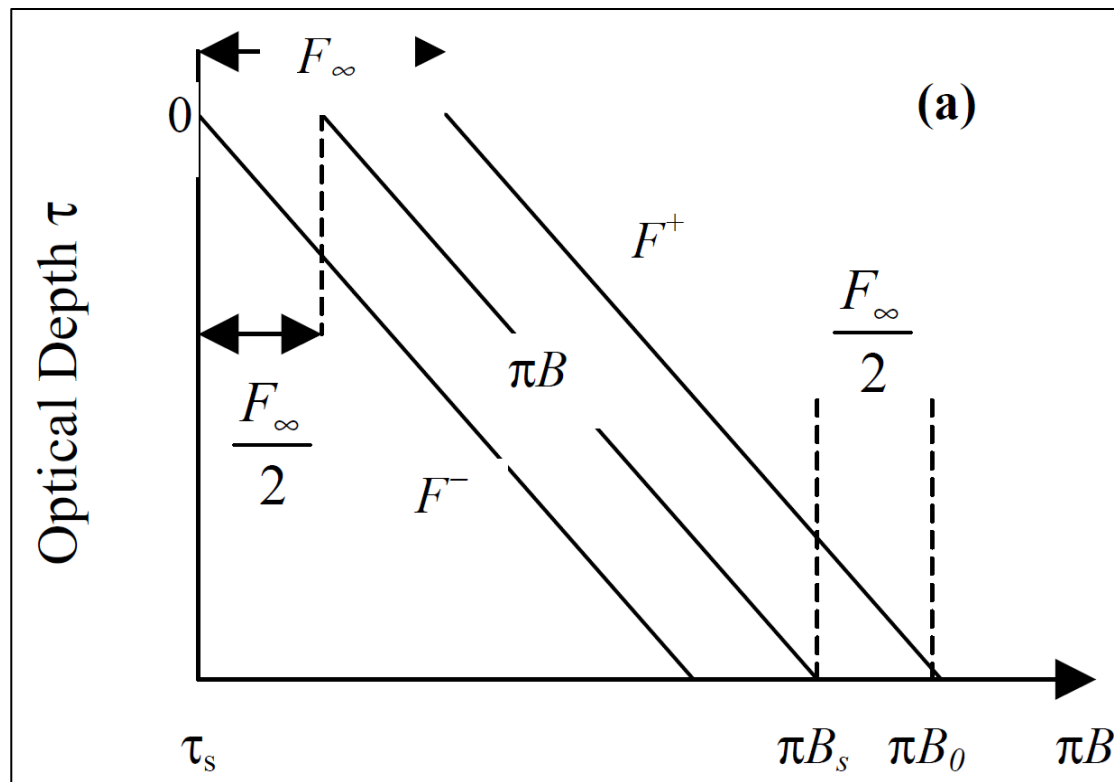
The solutions represented by Eqns. (6.10a) and (6.10b) provide rather interesting insights into the temperature profiles that are predicted by these equations. One of the results of this model is an estimate of the 'skin' temperature, which we think of as a measure of the stratospheric temperature. We obtain this using Eqn. (6.10a) with $\tilde{\tau} = 0$

$$\sigma T^4(\tilde{\tau} = 0) = \frac{F_\infty}{2}$$

and with $F_\infty \approx 235 \text{ Wm}^{-2}$, it follows that this temperature is $T_{skin} = [117.5/5.68 \times 10^{-8}]^{0.25} = 213 \text{ K}$.

The solutions in Eqns. (6.10a) and (6.10b) predict a discontinuity between the surface temperature T_s and the air temperature just above the ground $T(\tilde{\tau}_s)$. Differencing these equations and with $\tilde{\tau} = \tilde{\tau}_s$,

$$\sigma T_s^4 - \sigma T^4(\tilde{\tau}_s) = \frac{F_\infty}{2}.$$



“This radiative equilibrium profile is unstable w.r.t. vertical motion and is destroyed by convection.”

The surface has a net surplus of radiant energy compared to the bottom of the atmosphere, balanced by convection, being equal half of the effective emission in the clear-sky: $\sigma T_s^4 - \sigma T^4(\tau_s) = \frac{F_\infty}{2}$. Eq. (1) of Set 1

Deductions from a simple climate model: Factors governing surface temperature and atmospheric thermal structure

C. P. Weaver and V. Ramanathan

Center for Clouds, Chemistry and Climate, Scripps Institution of Oceanography, La Jolla, California

Temperature discontinuity. Equations (6a) and (6b) predict a temperature jump at the surface:

$$\sigma T_g^4 - \sigma T(\tau^*)^4 = \frac{f_0}{2} \quad (7)$$

Eq. (1) of Set 1

CERES EBAF-Surface Ed2.8 Data Quality Summary (March 27, 2015)

Table 4-1. Global annual mean fluxes using data from March 2000 through February 2010 (W m⁻²).

| | Flux Component | Ed3A SYN1deg -Month | EBAF- Surface Ed2.6r | EBAF- Surface Ed2.7 | EBAF- Surface Ed2.8 | EBAF- TOA Ed2.8 |
|---------|---------------------|---------------------------|----------------------------|---------------------------|---------------------------|-----------------------|
| TOA | Incoming solar | 339.9 | 339.9 | 339.9 | 339.8 | 339.8 |
| | LW (all-sky) | 237.3 | 239.7 | 239.6 | 239.6 | 239.6 |
| | SW (all-sky) | 98.5 | 99.6 | 99.6 | 99.6 | 99.6 |
| | Net (all-sky) | 4.06 | 0.64 | 0.69 | 0.63 | 0.59 |
| | LW (clear-sky) | 263.7 | 265.8 | 265.7 | 265.7 | 265.8 |
| | SW (clear-sky) | 52.5 | 52.5 | 52.6 | 52.6 | 52.6 |
| | Net (clear-sky) | 23.6 | 21.6 | 21.6 | 21.6 | 21.5 |
| Surface | LW down (all-sky) | 341.8 | 343.7 | 345.1 | 345.1 | |
| | LW up (all-sky) | 397.6 | 398.1 | 398.1 | 398.0 | |
| | SW down (all-sky) | 187.2 | 186.7 | 186.5 | 186.4 | |
| | SW up (all-sky) | 23.3 | 24.1 | 24.1 | 24.1 | |
| | Net (all-sky) | 108.1 | 108.3 | 109.4 | 109.4 | |
| | LW down (clear-sky) | 313.5 | 314.1 | 315.8 | 316.0 | |
| | LW up (clear-sky) | 396.6 | 398.3 | 398.4 | 398.0 | |
| | SW down (clear-sky) | 242.4 | 243.4 | 244.1 | 243.9 | |
| | SW up (clear-sky) | 28.7 | 29.6 | 29.7 | 29.7 | |
| | Net (clear-sky) | 130.6 | 129.6 | 131.8 | 132.2 | |

Eq. (1) **Surface Net (clear-sky) = TOA LW (clear-sky) / 2**
132.2 = 265.7 / 2

CERES EBAF-Surface Ed2.8 Data Quality Summary (March 27, 2015)

Table 4-1. Global annual mean fluxes using data from March 2000 through February 2010 (W m^{-2}).

| | Flux Component | Ed3A SYN1deg -Month | EBAF- Surface Ed2.6r | EBAF- Surface Ed2.7 | EBAF- Surface Ed2.8 | EBAF- TOA Ed2.8 |
|---------|---------------------|---------------------------|----------------------------|---------------------------|---------------------------|-----------------------|
| TOA | Incoming solar | 339.9 | 339.9 | 339.9 | 339.8 | 339.8 |
| | LW (all-sky) | 237.3 | 239.7 | 239.6 | 239.6 | 239.6 |
| | SW (all-sky) | 98.5 | 99.6 | 99.6 | 99.6 | 99.6 |
| | Net (all-sky) | 4.06 | 0.64 | 0.69 | 0.63 | 0.59 |
| | LW (clear-sky) | 263.7 | 265.8 | 265.7 | 265.7 | 265.8 |
| | SW (clear-sky) | 52.5 | 52.5 | 52.6 | 52.6 | 52.6 |
| | Net (clear-sky) | 23.6 | 21.6 | 21.6 | 21.6 | 21.5 |
| Surface | LW down (all-sky) | 341.8 | 343.7 | 345.1 | 345.1 | |
| | LW up (all-sky) | 397.6 | 398.1 | 398.1 | 398.0 | |
| | SW down (all-sky) | 187.2 | 186.7 | 186.5 | 186.4 | |
| | SW up (all-sky) | 23.3 | 24.1 | 24.1 | 24.1 | |
| | Net (all-sky) | 108.1 | 108.3 | 109.4 | 109.4 | |
| | LW down (clear-sky) | 313.5 | 314.1 | 315.8 | 316.0 | |
| | LW up (clear-sky) | 396.6 | 398.3 | 398.4 | 398.0 | |
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| | SW up (clear-sky) | 28.7 | 29.6 | 29.7 | 29.7 | |
| | Net (clear-sky) | 130.6 | 129.6 | 131.8 | 132.2 | |

Eq. (1) **Surface Net (clear-sky) = TOA LW (clear-sky) / 2 – Net (all-sky)**
132.2 = 265.7 / 2 – 0.65 Wm^{-2}

Inamdar and Ramanathan (1997, Tellus)

On monitoring the atmospheric greenhouse effect from space

"2 quantities are used as a measure of the atmospheric greenhouse effect: (1) G_a , which is the reduction in the clear sky outgoing longwave radiation (OLR) due to the atmosphere; it is the radiative heating of the surface-atmosphere column; (2) G_a^* , which is the back radiation from the atmosphere to the surface; it is the radiative heating of the surface by the atmosphere."

$$G_a = \sigma T(\tau^*)^4 - f_0$$

is the radiative heating of the surface-atmosphere column.

Eq. (1) says: The surface has a net surplus of radiant energy *compared to the bottom of the atmosphere*, balanced by convection, being equal $OLR/2$ in the clear-sky.

Eq. (2) follows from noting that the bottom of the atmosphere has also a net surplus of radiant energy *compared to the top-of-atmosphere, called the greenhouse effect*, balanced by the same convection as well, so this also equals $f_0/2$.

Using Eq. (1),

$$G_a = \sigma T(\tau^*)^4 - f_0 = CONV = \sigma T_g^4 - \sigma T(\tau^*)^4 = f_0/2.$$

Inamdar and Ramanathan (1997, Tellus)

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$$G_a = \sigma T(\tau^*)^4 - f_0$$

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Eq. (2) follows from noting that the bottom of the atmosphere has also a net surplus of radiant energy *compared to the top-of-atmosphere, called the greenhouse effect*, balanced by the same convection as well, so this also equals $f_0/2$.

Using Eq. (1),

$$G_a = \sigma T(\tau^*)^4 - f_0 = \text{CONV} = \sigma T_g^4 - \sigma T(\tau^*)^4 = f_0/2.$$

From here,

$$\sigma T(\tau^*)^4 = 3f_0/2 \quad \text{and} \quad \sigma T_g^4 = 2f_0 \quad \text{Eq. (2) of Set 1}$$

that is,

$$g_a = G_a/\sigma T(\tau^*)^4 = 1/3.$$

“the normalized g_a is 0.33, i.e., the atmosphere reduces the energy escaping to space by a factor of 1/3”
(Ramanathan and Inamdar 2006)

Eq. (1) derived from Eq. (2) in Hartmann Global Physical Climatology, Academic Press (1994, 2016)

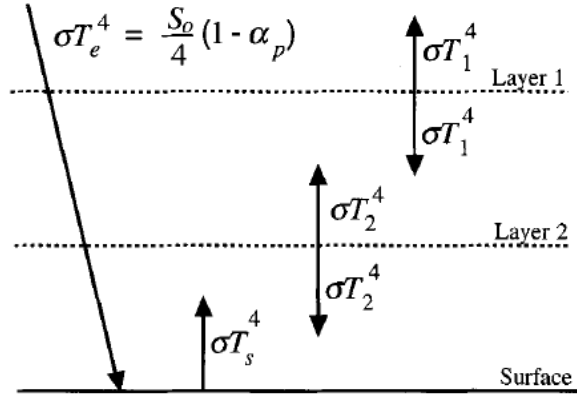


Fig. 3.10 Diagram of simple two-layer radiative equilibrium model for the atmosphere–Earth system, showing the fluxes of radiant energy.

And the balance at the surface is

$$\frac{S_0}{4} (1 - \alpha_p) + \sigma T_2^4 = \sigma T_s^4 \tag{3.50}$$

The critical effect of an atmosphere that absorbs and emits longwave radiation appears in (3.50). The energy supplied to the surface by the sun is augmented by a downward flux of longwave radiation from the atmosphere. This allows the surface temperature

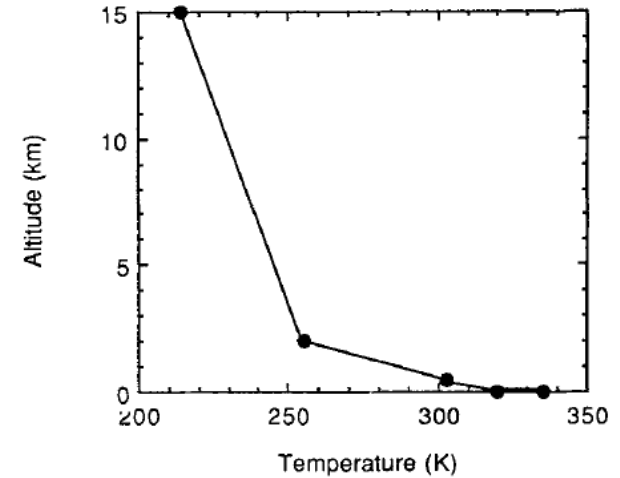


Fig. 3.11 Plot of temperature profile obtained from the simple two-level atmosphere radiative equilibrium model.

A thin layer of atmosphere near the surface absorbs a fraction ϵ of the emission from above and below and emits in both directions. The temperature of the air adjacent to the surface, T_{SA} , may be derived from the energy balance there.

$$\epsilon \sigma T_s^4 + \epsilon \sigma T_2^4 = 2 \epsilon \sigma T_{SA}^4 \tag{3.54}$$

$$\Rightarrow \sigma T_s^4 - \sigma T_{SA}^4 = \sigma T_e^4 / 2$$

CERES EBAF Ed2.8 Global means (Mar 2000 – Feb 2016)

Clear-sky

Rose et al., 27th STM (2017)

$$\text{Eq. (1) Surface Net} = \text{TOA LW Up} / 2$$
$$244.06 - 29.74 + 316.27 - 398.40 = 265.59 / 2 - 0.60 \text{ Wm}^{-2}$$

$$\text{Eq. (2) Surface Total} = 2 \times \text{TOA LW Up}$$
$$244.06 - 29.74 + 316.27 = 2 \times 265.59 - 0.59 \text{ Wm}^{-2}$$

| Clear Sky | Ed2.8 |
|-------------------|---------------|
| TOA SW Insolation | 339.87 |
| <i>TOA SW Up</i> | <i>52.50</i> |
| <i>TOA LW Up</i> | <i>265.59</i> |
| SFC SW Down | 244.06 |
| SFC SW Up | 29.74 |
| SFC LW Down | 316.27 |
| SFC LW Up | 398.40 |

CERES EBAF Ed2.8 Global means (Mar 2000 – Feb 2016)

Clear-sky

Rose et al., 27th STM (2017)

$$\text{Eq. (1) Surface Net} = \text{TOA LW Up} / 2$$
$$244.06 - 29.74 + 316.27 - 398.40 = 265.59 / 2 - 0.60 \text{ Wm}^{-2}$$

$$\text{Eq. (2) Surface Total} = 2 \times \text{TOA LW Up}$$
$$244.06 - 29.74 + 316.27 = 2 \times 265.59 - 0.59 \text{ Wm}^{-2}$$

$$\Rightarrow \text{Surface LW Up} = 3 \times \text{TOA LW Up} / 2$$
$$398.40 = 1.5 \times 265.59 - 0.01 \text{ Wm}^{-2}$$

| Clear Sky | Ed2.8 |
|-------------------|--------|
| TOA SW Insolation | 339.87 |
| <i>TOA SW Up</i> | 52.50 |
| <i>TOA LW Up</i> | 265.59 |
| SFC SW Down | 244.06 |
| SFC SW Up | 29.74 |
| SFC LW Down | 316.27 |
| SFC LW Up | 398.40 |

CERES EBAF Ed2.8 Global means (Mar 2000 – Feb 2016)

Clear-sky

Rose et al., 27th STM (2017)

Eq. (1) Surface Net = TOA LW Up / 2
 $244.06 - 29.74 + 316.27 - 398.40 = 265.59 / 2 - 0.60 \text{ Wm}^{-2}$

Eq. (2) Surface Total = 2 × TOA LW Up
 $244.06 - 29.74 + 316.27 = 2 \times 265.59 - 0.59 \text{ Wm}^{-2}$

=> Surface LW Up = 3 × TOA LW Up / 2
 $398.40 = 1.5 \times 265.59 - 0.01 \text{ Wm}^{-2}$

Surface Net : TOA LW Up : SFC LW Up : Surface Total
1 : **2** : **3** : **4**

For example
 133 : 266 : 399 : 532 (Wm⁻²)

| Clear Sky | Ed2.8 |
|-------------------|--------|
| TOA SW Insolation | 339.87 |
| <i>TOA SW Up</i> | 52.50 |
| <i>TOA LW Up</i> | 265.59 |
| SFC SW Down | 244.06 |
| SFC SW Up | 29.74 |
| SFC LW Down | 316.27 |
| SFC LW Up | 398.40 |

CERES_EBAF_Ed4.2.1_v3_200101-202512.nc (7 Apr 2026)

| | | | | |
|-----|-----------------|-----------------|---------------|---------------|
| 289 | 392,6669 | 263,6845 | 128,9824 | 0,328478 |
| 290 | 393,8643 | 264,3423 | 129,522 | 0,328849 |
| 291 | 397,2096 | 264,6787 | 132,5309 | 0,333655 |
| 292 | 401,2489 | 265,4551 | 135,7938 | 0,338428 |
| 293 | 405,2417 | 267,0644 | 138,1773 | 0,340975 |
| 294 | 408,5014 | 268,9221 | 139,5793 | 0,341686 |
| 295 | 410,0806 | 269,913 | 140,1676 | 0,341805 |
| 296 | 409,1639 | 269,5647 | 139,5992 | 0,341182 |
| 297 | 406,6477 | 268,4265 | 138,2212 | 0,339904 |
| 298 | 401,3641 | 266,4104 | 134,9537 | 0,336238 |
| 299 | 395,3934 | 264,207 | 131,1864 | 0,331787 |
| 300 | 392,0032 | 262,8878 | 129,1154 | 0,329373 |
| 301 | sfc_lw_up-clear | toa_lw_up_clear | G | g |
| 302 | 399,07 | 266,00 | 133,06 | 0,3333 |

| Clear-sky | N | Geometry | CERES |
|---------------|----------|----------|--------|
| Surface LW up | 3 | 399 | 399.07 |
| TOA LW up | 2 | 266 | 266.00 |
| G | 1 | 133 | 133.06 |
| g | 1/3 | 1/3 | 0.3333 |

Creating the all-sky versions

$$\text{Eq. (1) } R_N(\text{clear}) = \text{SFC} (\text{SW down} - \text{SW up} + \text{LW down} - \text{LW up})(\text{clear-sky}) = \text{TOA LW (clear-sky)}/2$$

$$\text{Eq. (2) } R_T(\text{clear}) = \text{SFC} (\text{SW down} - \text{SW up} + \text{LW down}) \quad (\text{clear-sky}) = \text{TOA LW (clear-sky)} \times 2$$

$$\text{Eq. (3) } R_N(\text{all}) = \text{SFC} (\text{SW down} - \text{SW up} + \text{LW down} - \text{LW up}) (\text{all-sky}) = \text{TOA} [\text{LW (all-sky)} - \text{LWCRE}]/2$$

$$\text{Eq. (4) } R_T(\text{all}) = \text{SFC} (\text{SW down} - \text{SW up} + \text{LW down}) \quad (\text{all-sky}) = \text{TOA LW (all-sky)} \times 2 + \text{LWCRE}$$

Verification of the four equations

CERES EBAF Ed4.1 Version 3, 22 years (April 2000 – March 2022) (Wm^{-2})

$$\begin{array}{l} \text{Eq. (1)} \quad \text{SFC SW down} - \text{SW up} + \text{LW down} - \text{LW up (clear)} = \text{TOA LW (clear)}/2 \\ \quad \quad \quad 240.8680 - 29.0724 + 317.4049 - 398.5211 \quad \quad \quad = 266.0122 /2 \quad \quad \quad - 2.3267 \end{array}$$

$$\begin{array}{l} \text{Eq. (2)} \quad \text{SFC SW down} - \text{SW up} + \text{LW down} \quad \quad \quad (\text{clear}) = 2 \times \text{TOA LW (clear)} \\ \quad \quad \quad 240.8680 - 29.0724 + 317.4049 \quad \quad \quad = 2 \times 266.0122 \quad \quad \quad - 2.8238 \end{array}$$

$$\begin{array}{l} \text{Eq. (3)} \quad \text{SFC SW down} - \text{SW up} + \text{LW down} - \text{LW up} \quad (\text{all}) = [\text{TOA LW (all)} - \text{LWCRE}]/2 \\ \quad \quad \quad 186.8544 - 23.1629 + 345.0108 - 398.7550 \quad \quad \quad = (240.2450 - 25.7672)/2 \quad \quad \quad + 2.7083 \end{array}$$

$$\begin{array}{l} \text{Eq. (4)} \quad \text{SFC SW down} - \text{SW up} + \text{LW down} \quad \quad \quad (\text{all}) = 2 \times \text{TOA LW (all)} + \text{LWCRE} \\ \quad \quad \quad 186.8544 - 23.1629 + 345.0108 \quad \quad \quad = 2 \times 240.2450 + 25.7672 \quad \quad \quad + 2.4450 \end{array}$$

Mean 0.0007

Verification of the four equations

CERES EBAF Ed4.1 Version 3, 22 years (April 2000 – March 2022) (Wm^{-2})

CERES EBAF Ed4.2.1 Version 3, 25 years (April 2000 – March 2025) (Wm^{-2})

| | | |
|---------|--|----------|
| Eq. (1) | SFC SW down – SW up + LW down – LW up (clear) = TOA LW (clear)/2 | |
| | 240.8680 – 29.0724 + 317.4049 – 398.5211 = 266.0122 /2 | – 2.3267 |
| | 240.4417 – 29.6710 + 318.2640 – 398.9301 = 266.0004 /2 | – 2.3531 |

| | | |
|---------|--|----------|
| Eq. (2) | SFC SW down – SW up + LW down (clear) = 2 × TOA LW (clear) | |
| | 240.8680 – 29.0724 + 317.4049 = 2 × 266.0122 | – 2.8238 |
| | 240.4417 – 29.6710 + 318.2640 = 2 × 266.0004 | – 2.4236 |

| | | |
|---------|--|----------|
| Eq. (3) | SFC SW down – SW up + LW down – LW up (all) = [TOA LW (all) – LWCRE]/2 | |
| | 186.8544 – 23.1629 + 345.0108 – 398.7550 = (240.2450 – 25.7672)/2 | + 2.7083 |
| | 187.1294 – 23.4327 + 346.4731 – 398.7367 = (240.4417 – 25.5587)/2 | + 3.9915 |

| | | |
|---------|--|----------|
| Eq. (4) | SFC SW down – SW up + LW down (all) = 2 × TOA LW (all) + LWCRE | |
| | 186.8544 – 23.1629 + 345.0108 = 2 × 240.2450 + 25.7672 | + 2.4450 |
| | 187.1294 – 23.4327 + 346.4731 = 2 × 240.4417 + 25.5587 | + 3.7276 |

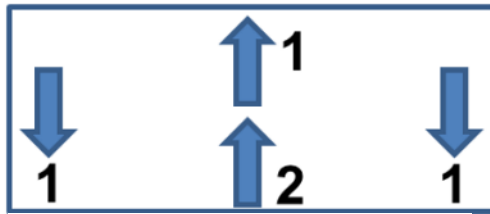
| | |
|------|--------|
| Mean | 0.0007 |
| | 0.7356 |

The **N**-numbers as solution of the equations

Pure geometry

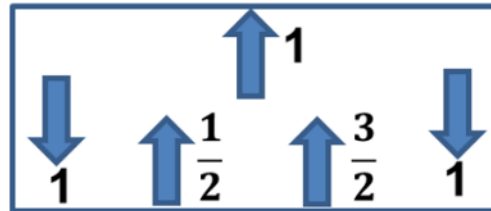
1 : 2 : 3 : 4

No reference to GHGs



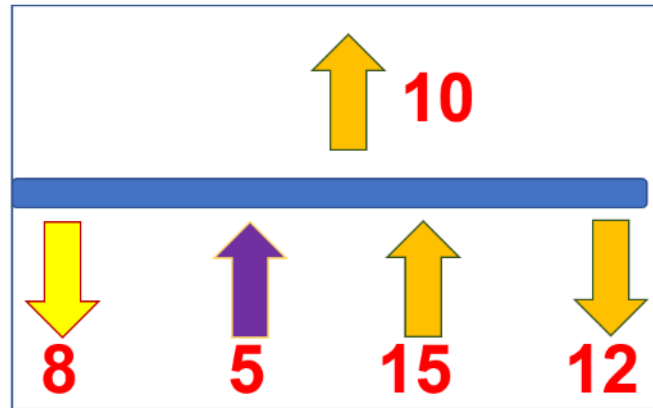
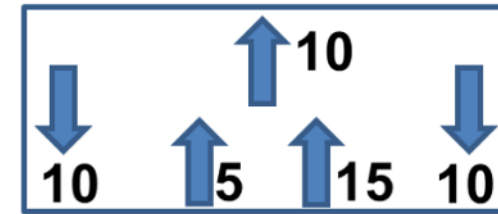
Eq.(2) SFC Tot = 2OLR

=>



(Clear-sky) Eq.(1) SFC Net = OLR/2

=



$$8 + 12 - 15 = 10 / 2$$

$$8 + 12 = 10 \times 2$$

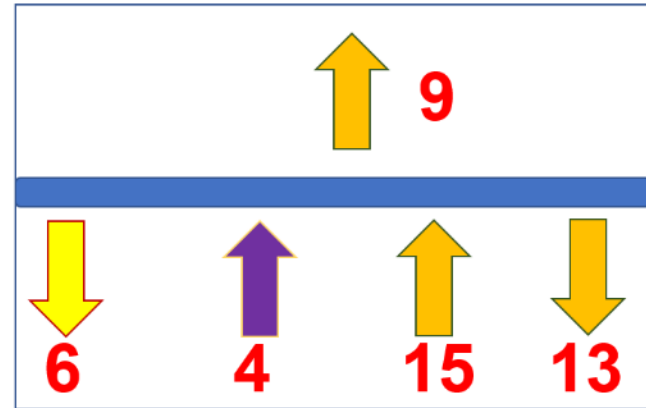
Eq. (1) SFC Net = OLR / 2

Eq. (2) SFC Tot = 2OLR

Clear-sky

L = 1

=>



$$6 + 13 - 15 = (9 - 1) / 2$$

$$6 + 13 = 9 \times 2 + 1$$

Eq. (3) SFC Net = (OLR - L) / 2

Eq. (4) SFC Tot = 2OLR + L

All-sky

The flux components with LWCRE = 1

| | | | |
|---------------------|-----------------------|----------------------|---------------------|
| TOA LW | clear-sky = 10 | TOA LW | all-sky = 9 |
| SFC LW up | clear-sky = 15 | SFC LW up | all-sky = 15 |
| SFC LW down | clear-sky = 12 | SFC LW down | all-sky = 13 |
| SFC LW net | clear-sky = -3 | SFC LW net | all-sky = -2 |
| SFC SW net | clear-sky = 8 | SFC SW net | all-sky = 6 |
| SFC SW+LW net | clear-sky = 5 | SFC SW+LW net | all-sky = 4 |
| SFC SW+LW total | clear-sky = 20 | SFC SW+LW total | all-sky = 19 |
| G greenhouse effect | clear-sky = 5 | G greenhouse effect | all-sky = 6 |
| SWCRE (surface) | = -2 | LWCRE (surface, TOA) | = 1 |

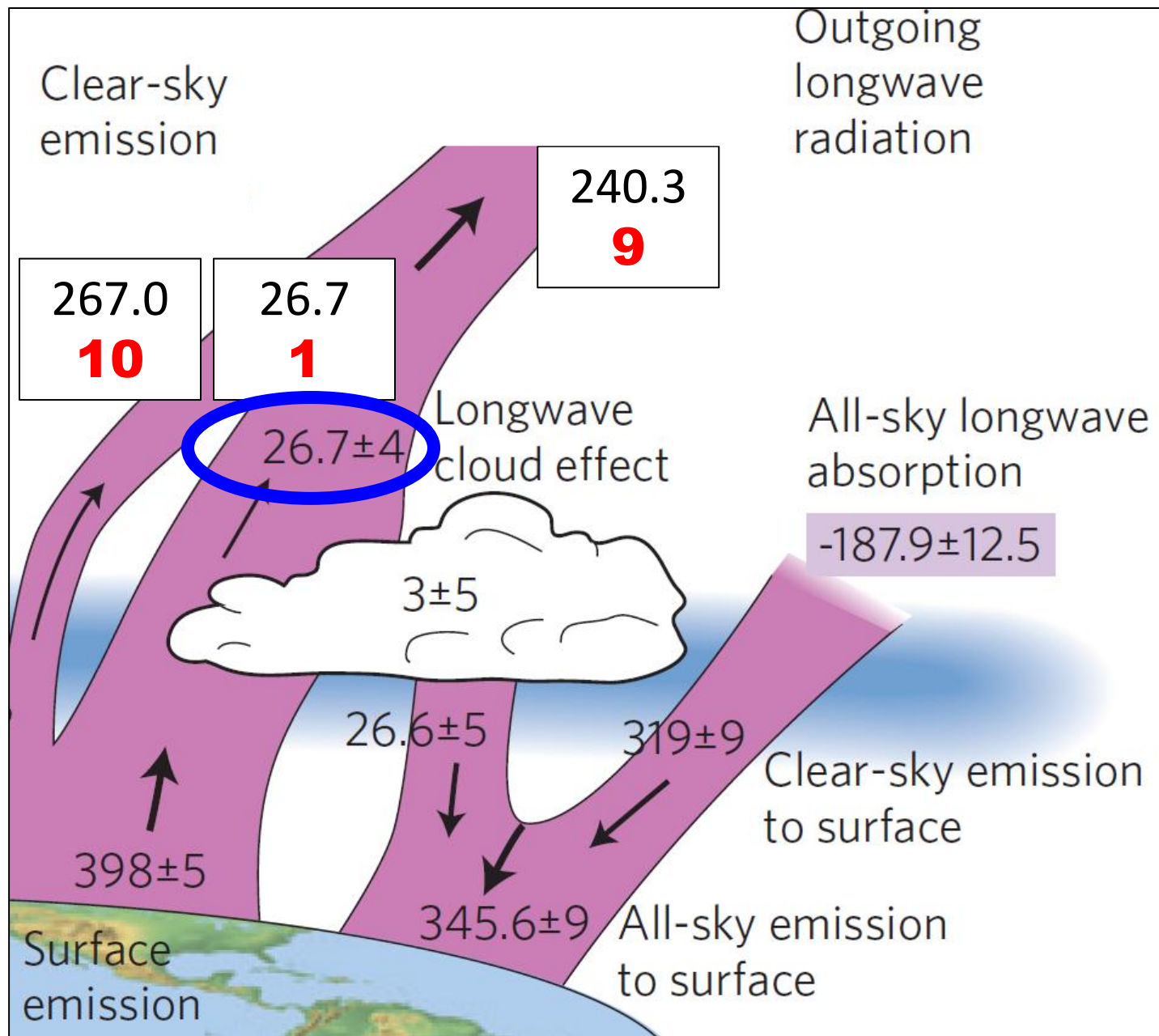
The flux components with LWCRE = 1

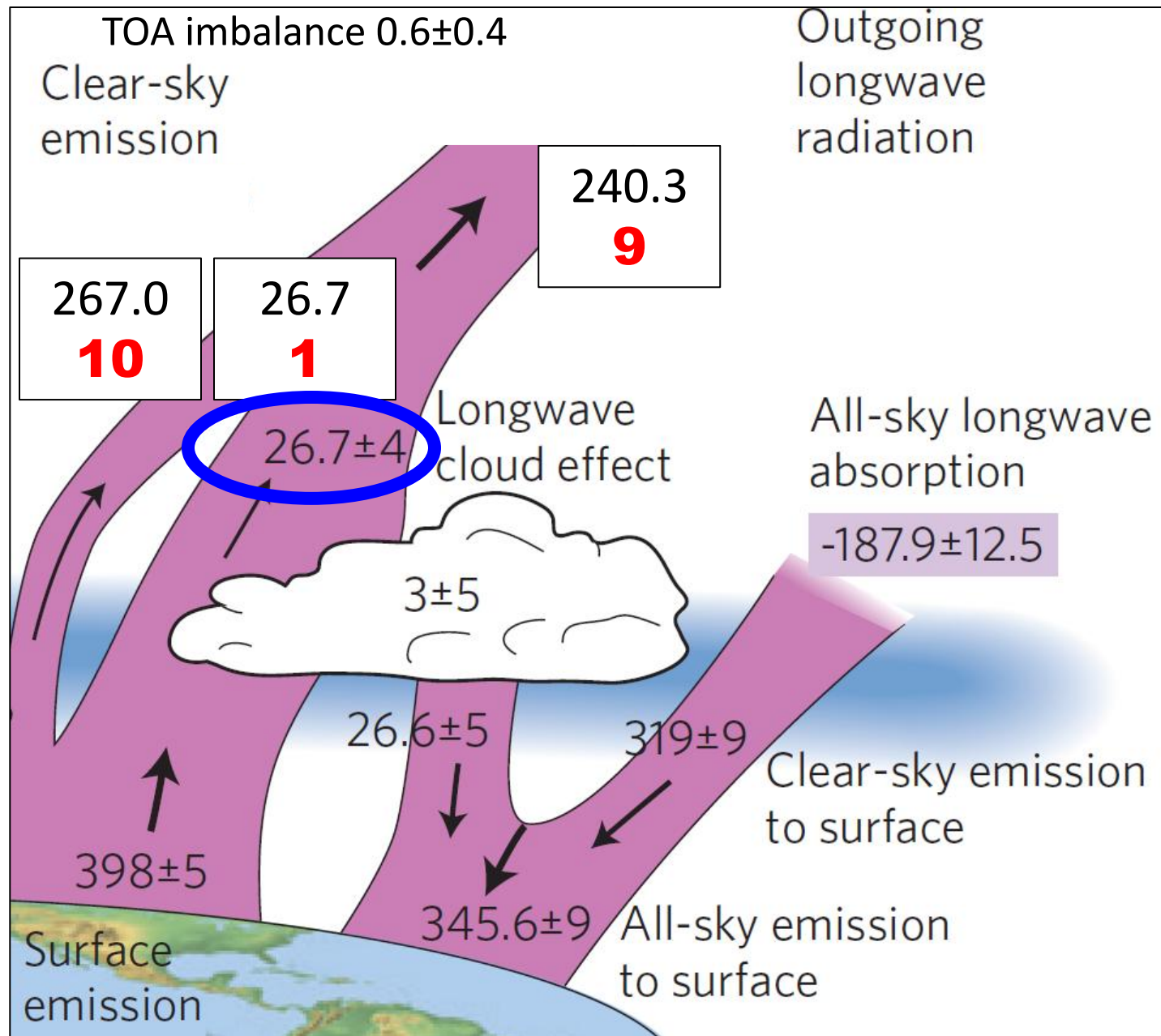
TOA LW

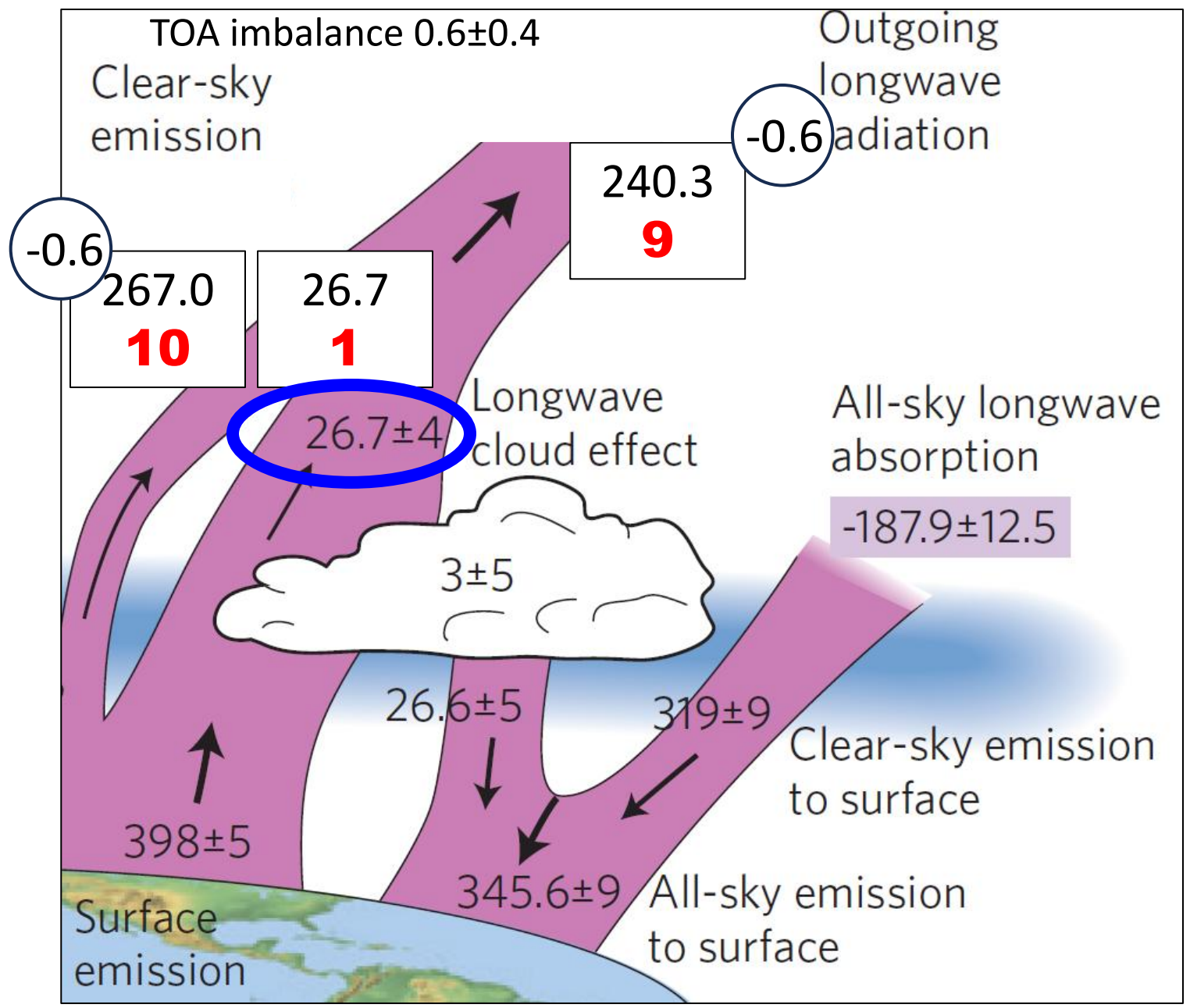
clear-sky = **10**

TOA LW

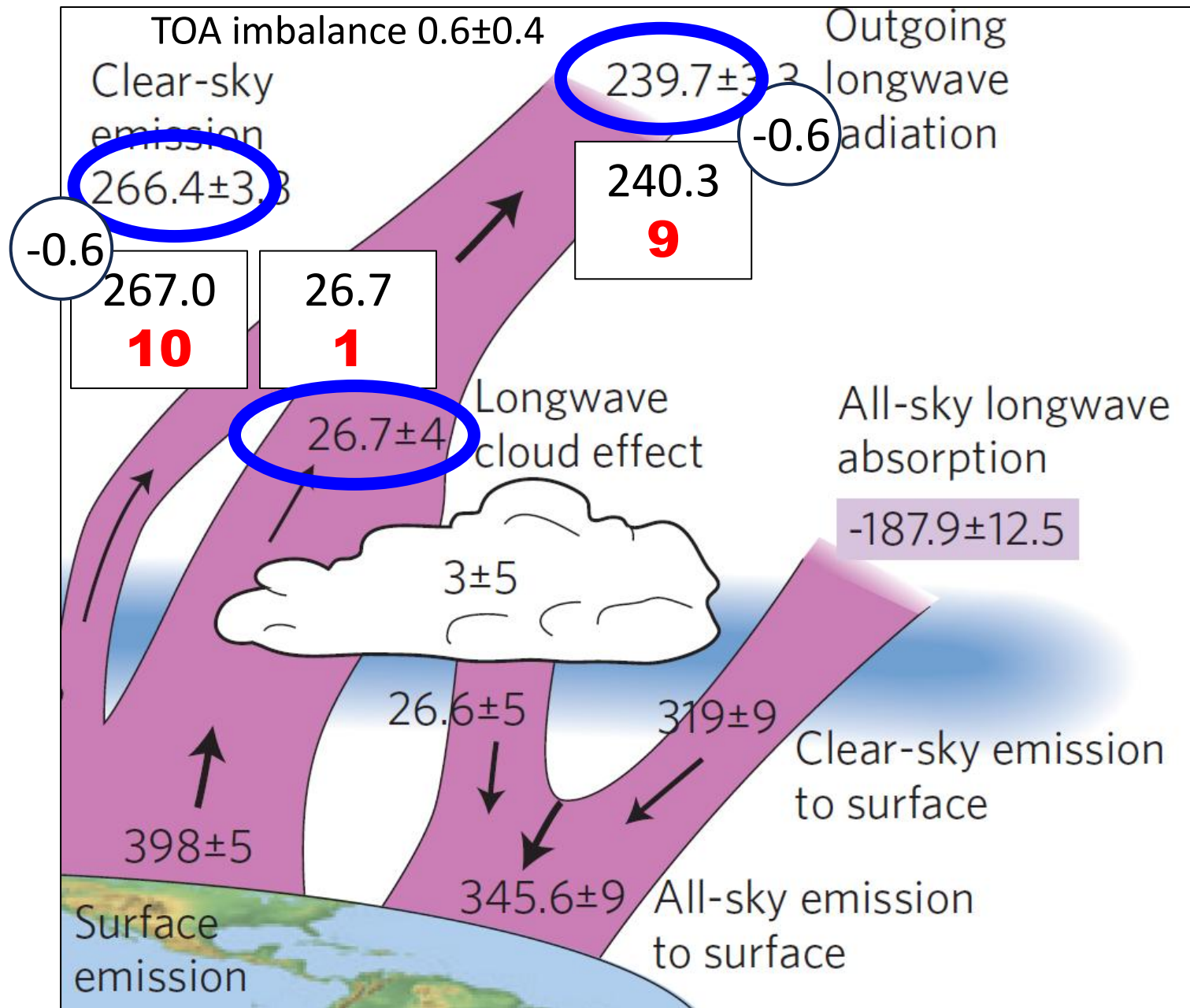
all-sky = **9**







Stephens et al.
(2012)



The flux components with LWCRE = 1

TOA LW

clear-sky = **10**

TOA LW

all-sky = **9**

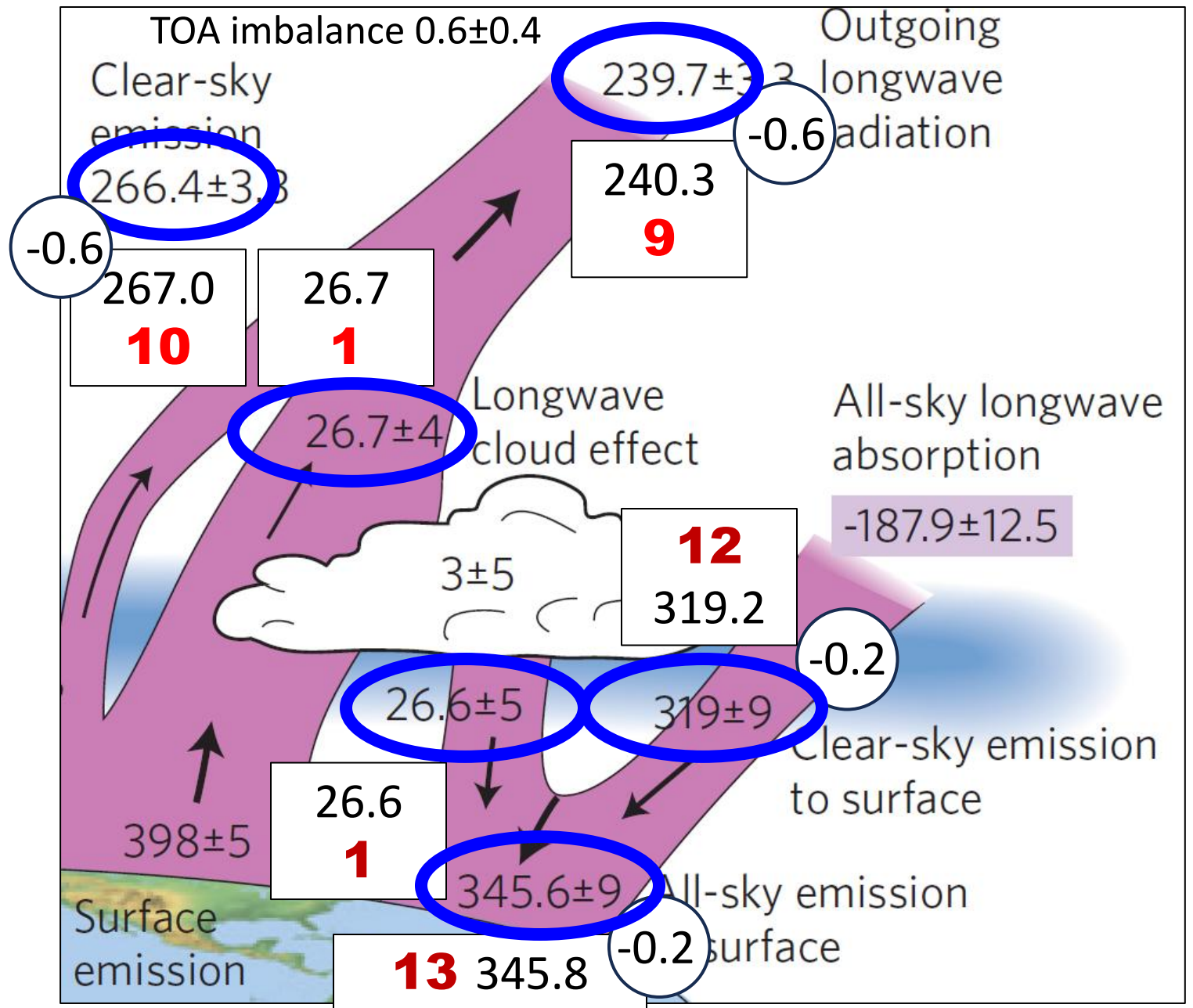
SFC LW down

clear-sky = **12**

SFC LW down

all-sky = **13**

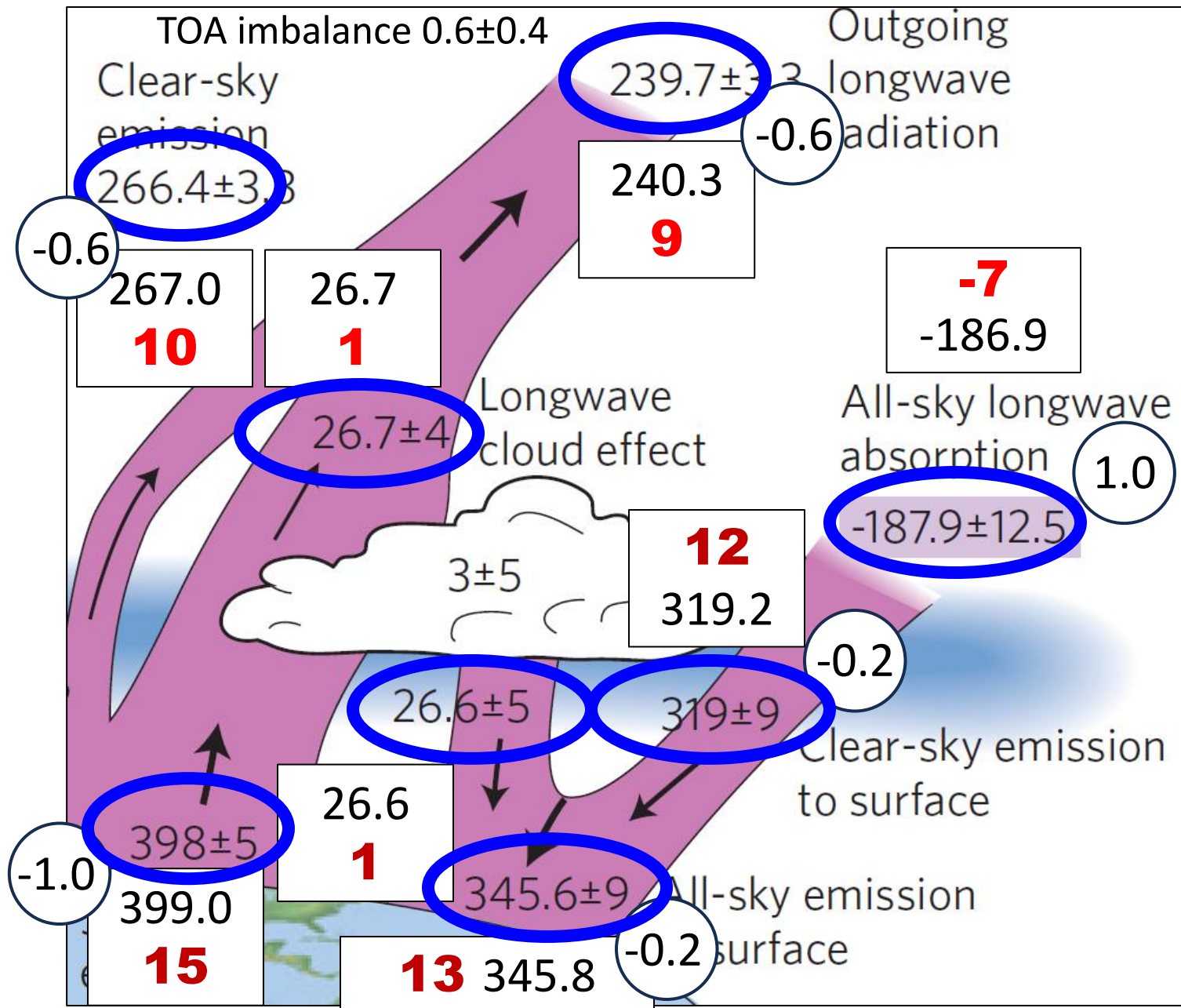
Stephens et al.
(2012)



The flux components with LWCRE = 1

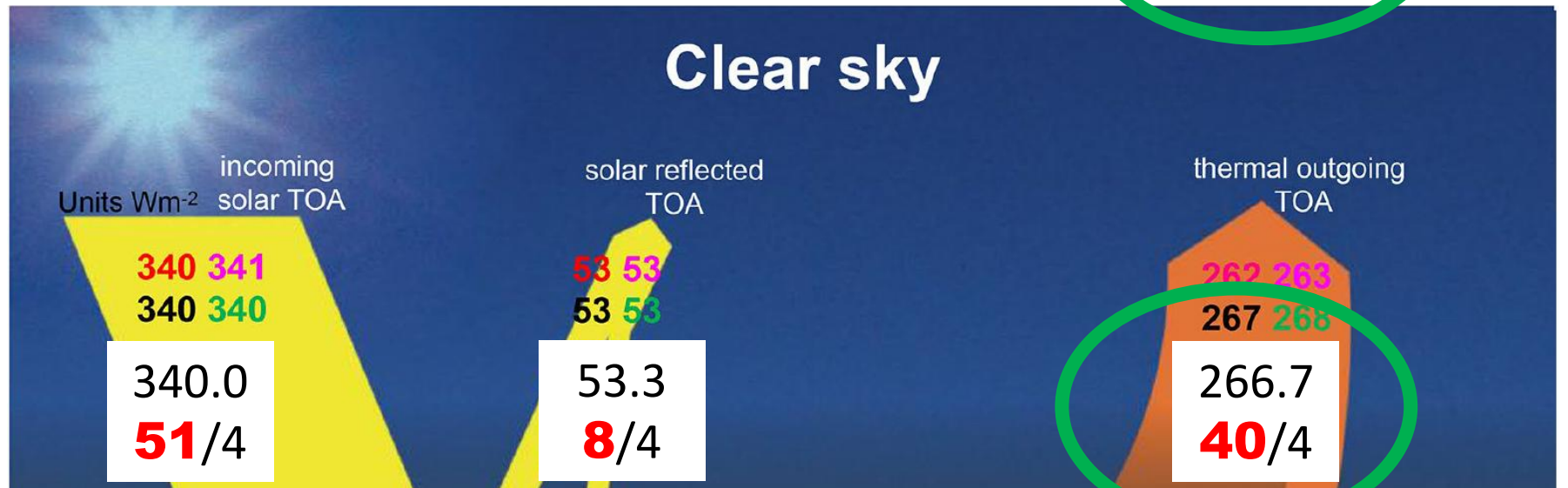
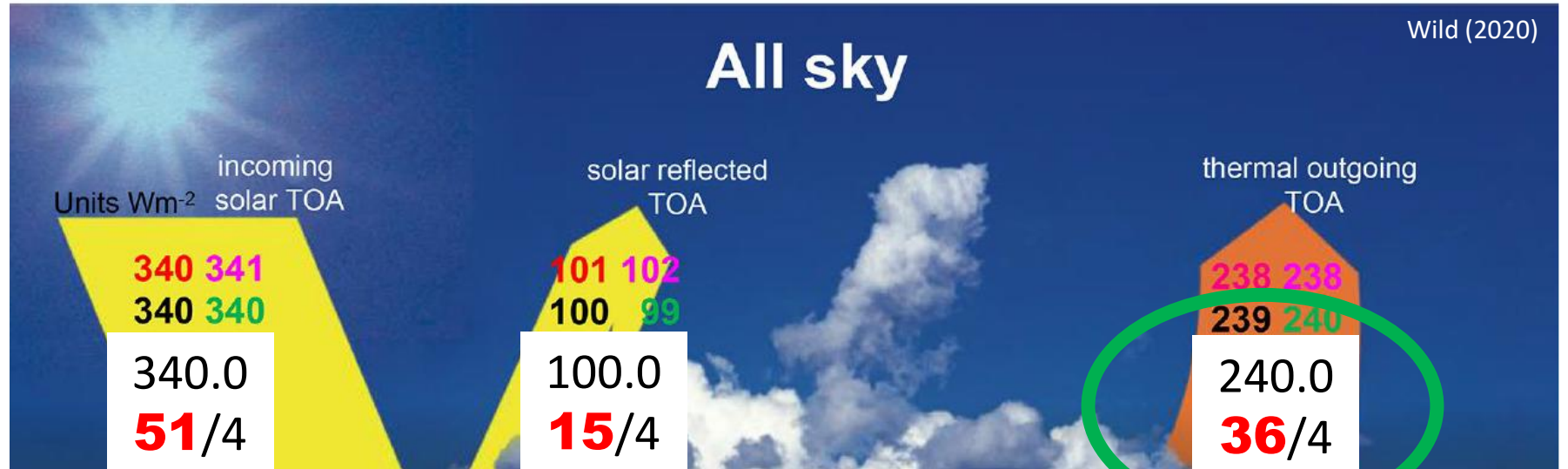
| | | | |
|----------------|-----------------------|----------------|---------------------|
| TOA LW | clear-sky = 10 | TOA LW | all-sky = 9 |
| SFC LW down | clear-sky = 12 | SFC LW down | all-sky = 13 |
| SFC LW up | clear-sky = 15 | SFC LW up | all-sky = 15 |
| ATM LW cooling | clear-sky = -7 | ATM LW cooling | all-sky = -7 |

Stephens et al.
(2012)



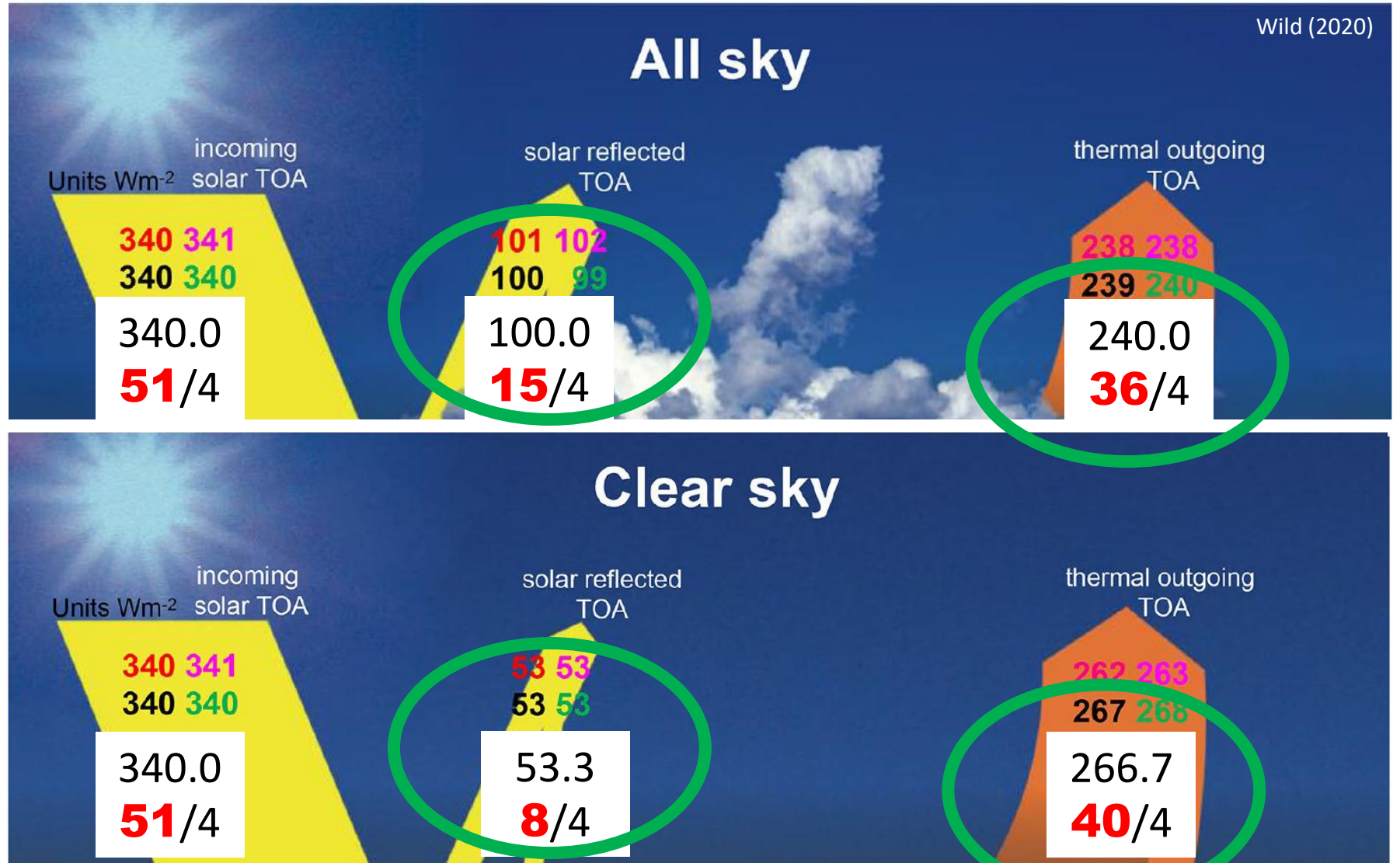
Extension: TOA

We already have $OLR(\text{all}) = 9 = 36/4$ and $OLR(\text{clear}) = 10 = 40/4$



Extension: TOA

We observe $RSW(\text{all}) = 15/4$ and $RSW(\text{clear}) = 2 = 8/4$

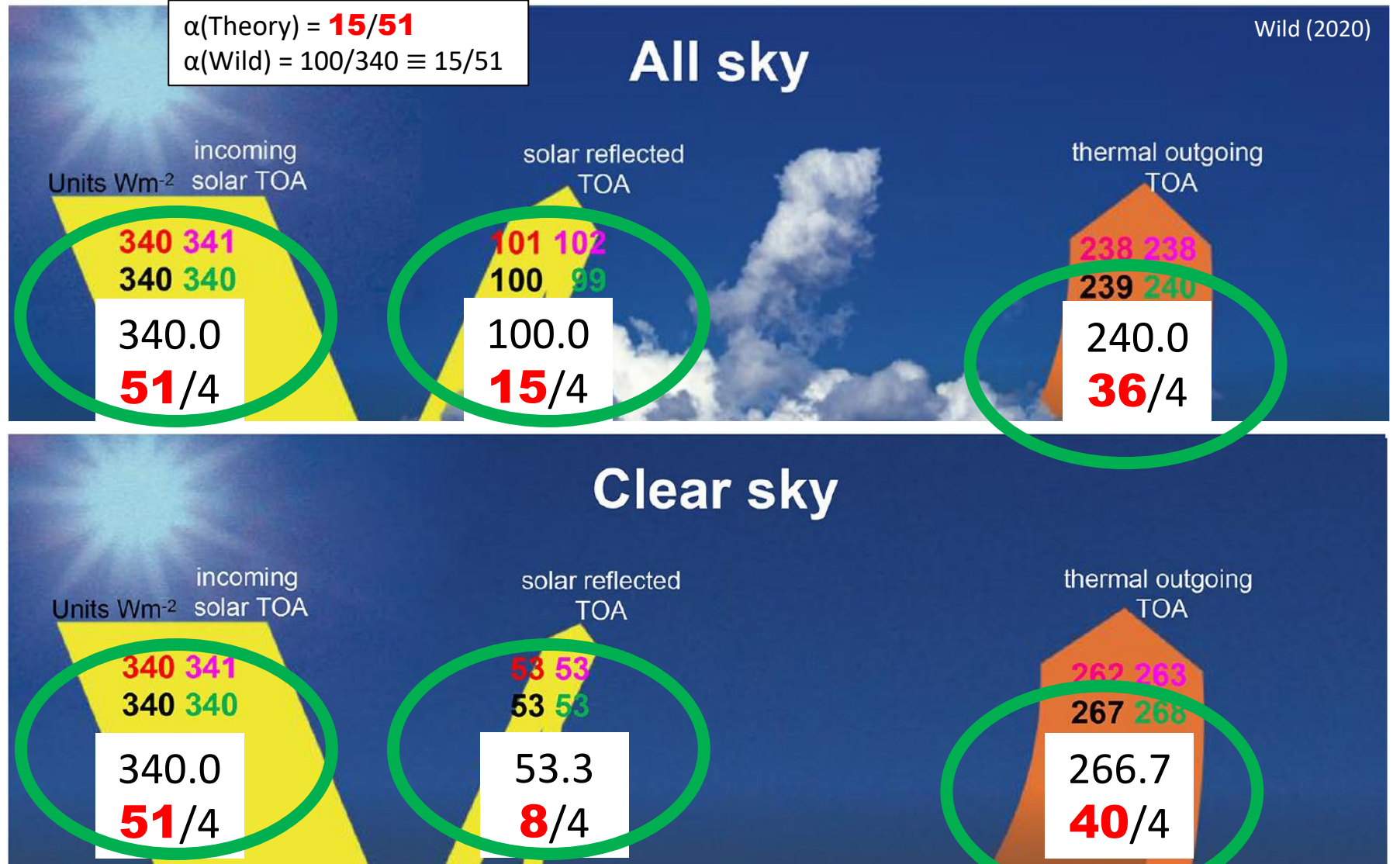
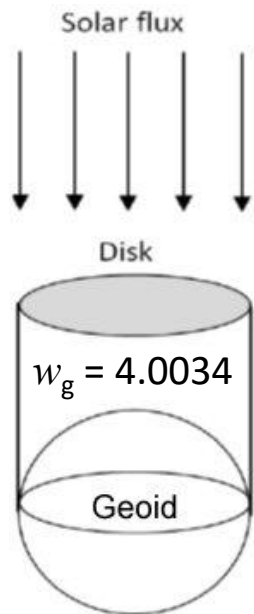


Extension: TOA

We infer $ISR = 51/4$ and $TSI = 51 \Rightarrow \alpha_p = 15/51$

The only input parameter is

TSI
51

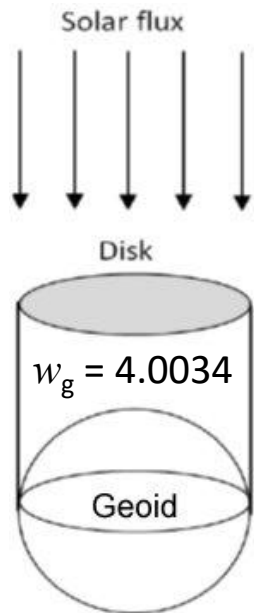


Extension: TOA

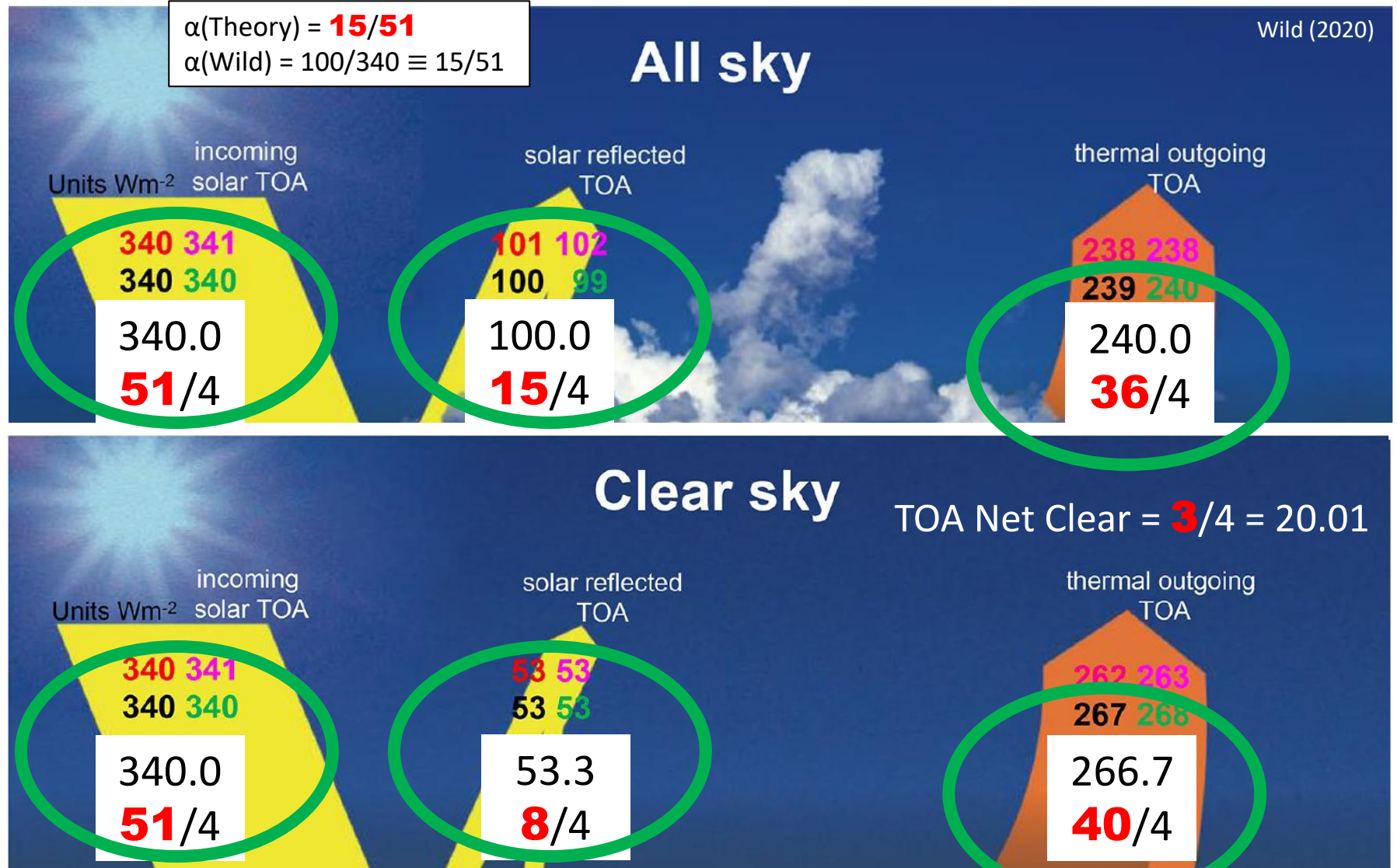
We infer TOA Net Clear = $3/4$ and TOA Net CRE = $-3/4 = -20.01 \text{ Wm}^{-2}$

The only input parameter is

TSI
51



1 = $26.684 \pm 0.01 \text{ Wm}^{-2}$

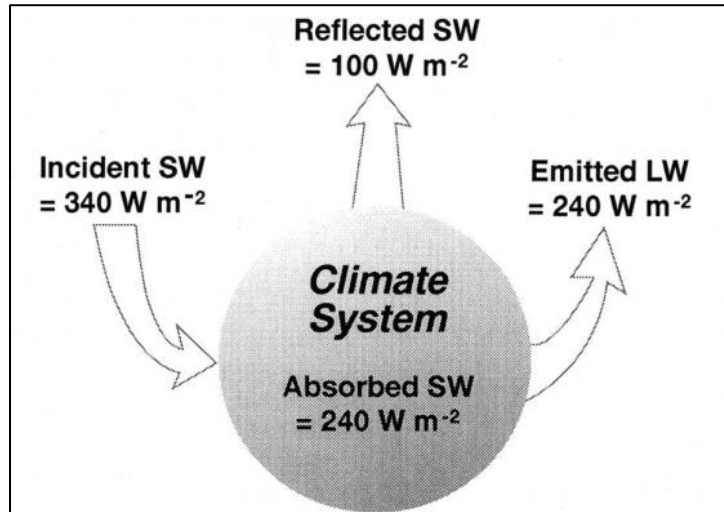


TOA All-sky, Albedo and TOA NET CRE were exact already in 1995

Mission to Planet Earth: Role of Clouds and Radiation in Climate

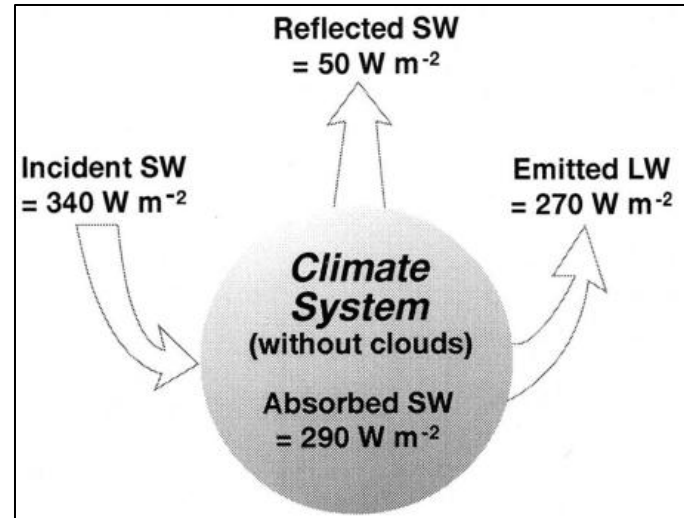
Bruce A. Wielicki,*
Robert D. Cess,+
Michael D. King,#
David A. Randall,@
and Edwin F. Harrison*

$\alpha(\text{Theory}) = \mathbf{15/51}$
 $\alpha(\text{Wielicki}) = 100/340 \equiv 15/51$



All-sky

Incident SW = 340 Wm⁻² = **51/4**
 Reflected SW = 100 Wm⁻² = **15/4**
 Absorbed SW = 240 Wm⁻² = **36/4**
 Emitted LW = 240 Wm⁻² = **36/4**



Clear-sky

Incident SW = 340 Wm⁻² = **51/4**
 Reflected SW = 53.33 Wm⁻² = **8/4**
 Absorbed SW = 286.67 Wm⁻² = **43/4**
 Emitted LW = 266.66 Wm⁻² = **40/4**

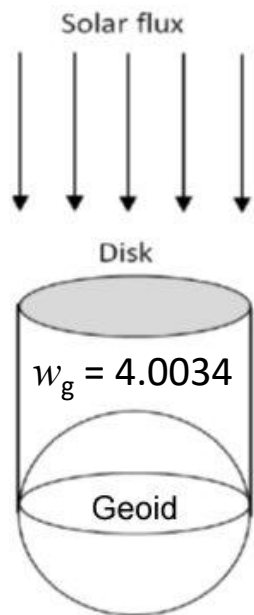
LW CRF = 26.68 Wm⁻² = **1**
 SW CRF = -46.69 Wm⁻² = **-7/4**
 NET CRF = -20.01 Wm⁻² = **-3/4**

Cloud-Radiative Forcing (CRF)
 LW CRF = 30 W m⁻²
 SW CRF = -50 W m⁻²
 NET CRF = -20 W m⁻²

The only input parameter is

TSI

51



1 = $26.684 \pm 0.01 \text{ Wm}^{-2}$

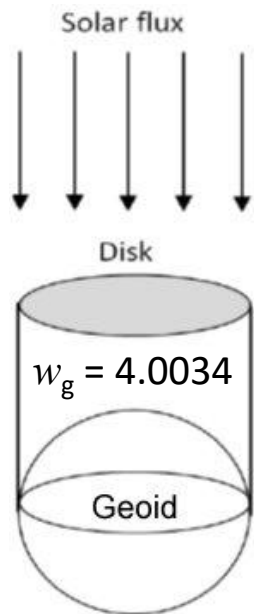
Extension: Surface SW down all-sky

Set 2

| | | | | |
|----------------|--|--|--------------------------------------|--------------------------------------|
| Surface | | | Kato et al. (2025) Edition 4.2 | Kato et al. (2025) Edition 4.1 |
| SW down all | | | 187.0 | 186.6 |
| | | | | |

The only input parameter is

TSI
51



1 = $26.684 \pm 0.01 \text{ Wm}^{-2}$

Extension: Surface SW down all-sky

Set 1

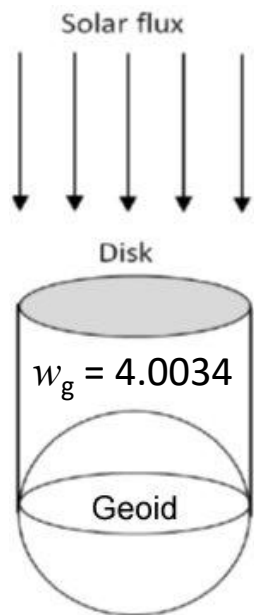
Set 2

| Surface | N | N × Unit | Kato et al. (2025) Edition 4.2 | Kato et al. (2025) Edition 4.1 |
|-------------|----------|-----------------|--------------------------------|--------------------------------|
| SW down all | 7 | 186.79 | 187.0 | 186.6 |
| | | | | |

The only input parameter is

TSI

51



1 = $26.684 \pm 0.01 \text{ Wm}^{-2}$

Extension: Surface SW down clear-sky

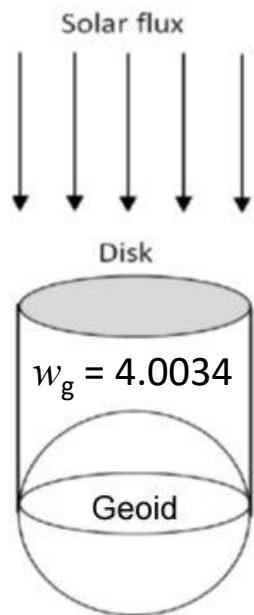
Set 2

| Surface | N | N × Unit | Kato et al. (2025) Edition 4.2 | Kato et al. (2025) Edition 4.1 |
|---------------|----------|-----------------|--------------------------------|--------------------------------|
| SW down all | 7 | 186.79 | 187.0 | 186.6 |
| SW down clear | | | 241.1 | 240.7 |

The only input parameter is

TSI

51



Extension: Surface SW down clear-sky

Set 1

Set 2

| Surface | N | N × Unit | Kato et al. (2025) Edition 4.2 | Kato et al. (2025) Edition 4.1 |
|---------------|----------|-----------------|--------------------------------|--------------------------------|
| SW down all | 7 | 186.79 | 187.0 | 186.6 |
| SW down clear | 9 | 240.16 | 241.1 | 240.7 |

1 = $26.684 \pm 0.01 \text{ Wm}^{-2}$

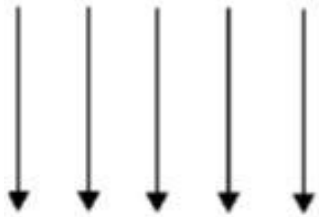
Set 1 and Set 2 of CERES Data Products, TOA



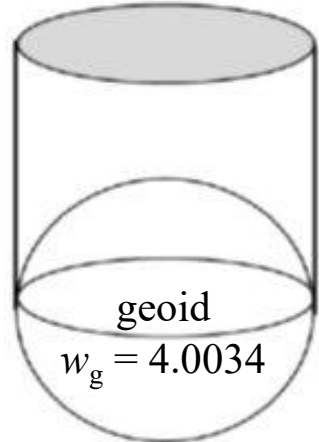
The only input parameter

51

Solar flux



Disk



| 1 = 26.684 Wm ⁻² | Set 1 | | Set 2 | Difference |
|------------------------------------|--------------|-----------------|--|--------------------------------------|
| TOA | N | N × Unit | EBAF Ed4.2.1_v3 Jan 2001 – Dec 2025 | Set 2 – Set 1 (Wm ⁻²) |
| Solar | 51 /4 | 340.22 | 340.22 | 0.00 |
| SW up clear | 8 /4 | 53.37 | 53.73 | 0.36 |
| LW up clear | 40 /4 | 266.84 | 266.00 | -0.84 |
| Net clear | 3 /4 | 20.01 | 20.49 | 0.48 |
| SW up all | 15 /4 | 100.06 | 98.83 | -1.23 |
| LW up all | 36 /4 | 240.15 | 240.48 | 0.33 |
| Net all | 0 | 0 | 0.90 | 0.90 |
| SW CRE | -7 /4 | -46.70 | -45.10 | 1.60 |
| LW CRE | 4 /4 | 26.684 | 25.52 | -1.17 |
| Net CRE | -3 /4 | -20.01 | -19.58 | 0.43 |

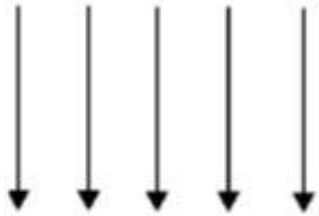
I infer that Set 1 is exact and Set 2 is accurate



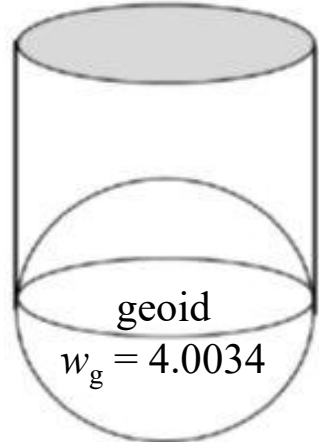
The only input parameter

51

Solar flux



Disk



| 1 = 26.684 Wm ⁻² | Set 1 | | Set 2 | Difference |
|------------------------------------|--------------|-----------------|--|--------------------------------------|
| TOA | N | N × Unit | EBAF Ed4.2.1_v3 Jan 2001 – Dec 2025 | Set 2 – Set 1 (Wm ⁻²) |
| Solar | 51 /4 | 340.22 | 340.22 | 0.00 |
| SW up clear | 8 /4 | 53.37 | 53.73 | 0.36 |
| LW up clear | 40 /4 | 266.84 | 266.00 | -0.84 |
| Net clear | 3 /4 | 20.01 | 20.49 | 0.48 |
| SW up all | 15 /4 | 100.06 | 98.83 | -1.23 |
| LW up all | 36 /4 | 240.15 | 240.48 | 0.33 |
| Net all | 0 | 0 | 0.90 | 0.90 |
| SW CRE | -7 /4 | -46.70 | -45.10 | 1.60 |
| LW CRE | 4 /4 | 26.684 | 25.52 | -1.17 |
| Net CRE | -3 /4 | -20.01 | -19.58 | 0.43 |

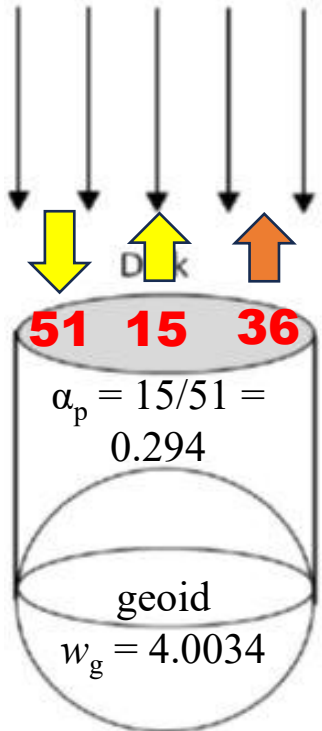
Notice that Set 1 TOA works on the disk



The only input parameter

51

Solar flux



| 1 = 26.684 Wm ⁻² | Set 1 | | Set 2 | Difference |
|------------------------------------|--------------|-----------------|--|--------------------------------------|
| TOA | N | N × Unit | EBAF Ed4.2.1_v3 Jan 2001 – Dec 2025 | Set 2 – Set 1 (Wm ⁻²) |
| Solar | 51/4 | 340.22 | 340.22 | 0.00 |
| SW up clear | 8/4 | 53.37 | 53.73 | 0.36 |
| LW up clear | 40/4 | 266.84 | 266.00 | -0.84 |
| Net clear | 3/4 | 20.01 | 20.49 | 0.48 |
| SW up all | 15/4 | 100.06 | 98.83 | -1.23 |
| LW up all | 36/4 | 240.15 | 240.48 | 0.33 |
| Net all | 0 | 0 | 0.90 | 0.90 |
| SW CRE | -7/4 | -46.70 | -45.10 | 1.60 |
| LW CRE | 4/4 | 26.684 | 25.52 | -1.17 |
| Net CRE | -3/4 | -20.01 | -19.58 | 0.43 |

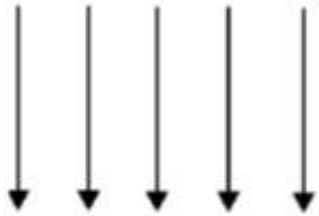
Set 1 and Set 2 of CERES Data Products, Surface



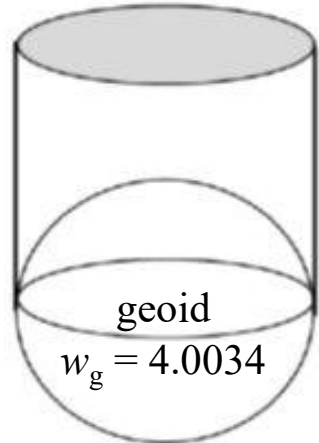
The only input parameter

51

Solar flux



Disk



| 1 = 26.684 Wm ⁻² | Set 1 | | Set 2 | Difference |
|------------------------------------|--------------|-----------------|-------------------------------------|--|
| Surface | N | N × Unit | EBAF Ed4.2.1 Jan 2001 – Dec 2025 | Set 2 – Set 1 (Wm⁻²) |
| SW down clear | 9 | 240.15 | 240.94 | 0.79 |
| SW up clear | 1 | 26.68 | 29.63 | 2.95 |
| SW net clear | 8 | 213.46 | 211.31 | -2.15 |
| LW down clear | 12 | 320.20 | 318.43 | -1.77 |
| LW up clear | 15 | 400.25 | 399.07 | -1.18 |
| LW net clear | -3 | -80.05 | -80.64 | -0.59 |
| Total net clear | 5 | 133.42 | 130.67 | -2.75 |
| SW down all | 7 | 186.78 | 187.12 | 0.34 |
| SW up all | 1 | 26.68 | 23.40 | -3.28 |
| SW net all | 6 | 160.10 | 163.72 | 3.62 |
| LW down all | 13 | 346.84 | 346.60 | -0.24 |
| LW up all | 15 | 400.20 | 398.87 | -1.33 |
| LW net all | -2 | -53.37 | -52.28 | 1.09 |
| Total net all | 4 | 106.73 | 111.44 | 4.71 |

If Libera will be a *"wohltemperierte Klavier"* => Set 3



A well-calibrated instrument

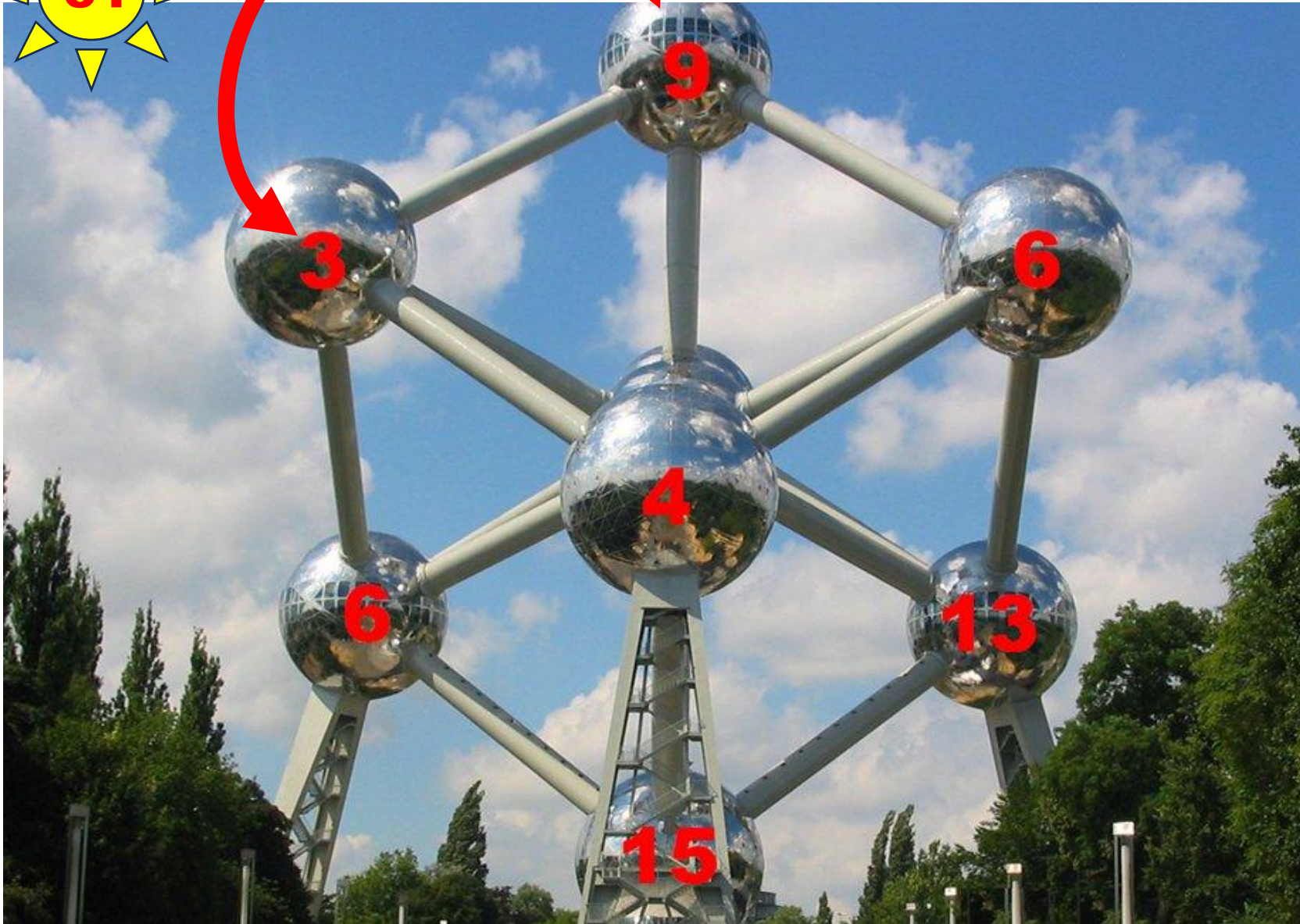
| 1 = 26.684 Wm ⁻² | Set 1 | | Set 2 | Set 3 | = Set 2 - Set 1 |
|---------------------------------------|--------------|-----------------|---------------|--|-------------------------------|
| TOA | N | N × Unit | Libera ? | Difference = Absolute Magnitude !!! | |
| Solar | 51 /4 | 340.22 | 340.22 | 0.00 | Zero (by def.) |
| SW up clear | 8 /4 | 53.37 | 53.73 | + 0.36 | Clear-sky SW Deviation |
| LW up clear | 40 /4 | 266.84 | 266.00 | - 0.84 | Clear-sky LW Deviation |
| Net clear | 3 /4 | 20.01 | 20.49 | + 0.48 | Net Clear-sky Deviation |
| SW up all | 15 /4 | 100.06 | 98.83 | - 1.23 | All-sky SW Deviation |
| LW up all | 36 /4 | 240.15 | 240.48 | + 0.33 | All-sky LW Deviation |
| Net all | 0 | 0 | 0.90 | + 0.90 | Net All-sky Deviation ("EEI") |
| SW CRE | -7 /4 | -46.70 | -45.10 | + 1.60 | SW CRE Deviation |
| LW CRE | 4 /4 | 26.684 | 25.52 | - 1.17 | LW CRE Deviation |
| Net CRE | -3 /4 | -20.01 | -19.58 | + 0.43 | Net CRE Deviation |

If Libera will be a well-calibrated instrument, it will measure absolute deviations from the equilibrium positions.



Set 1

Equilibrium positions



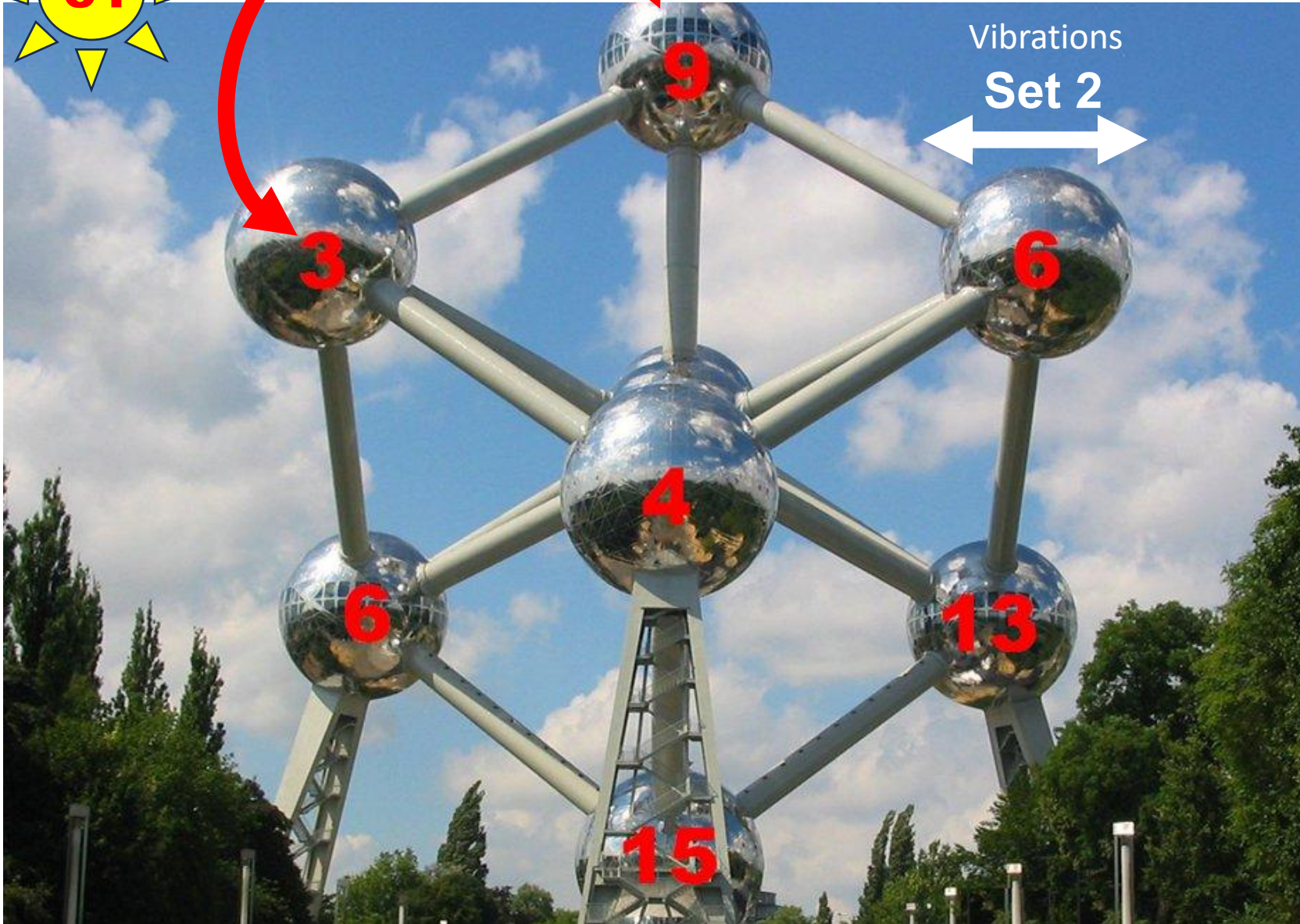


Set 1

Equilibrium positions

Vibrations

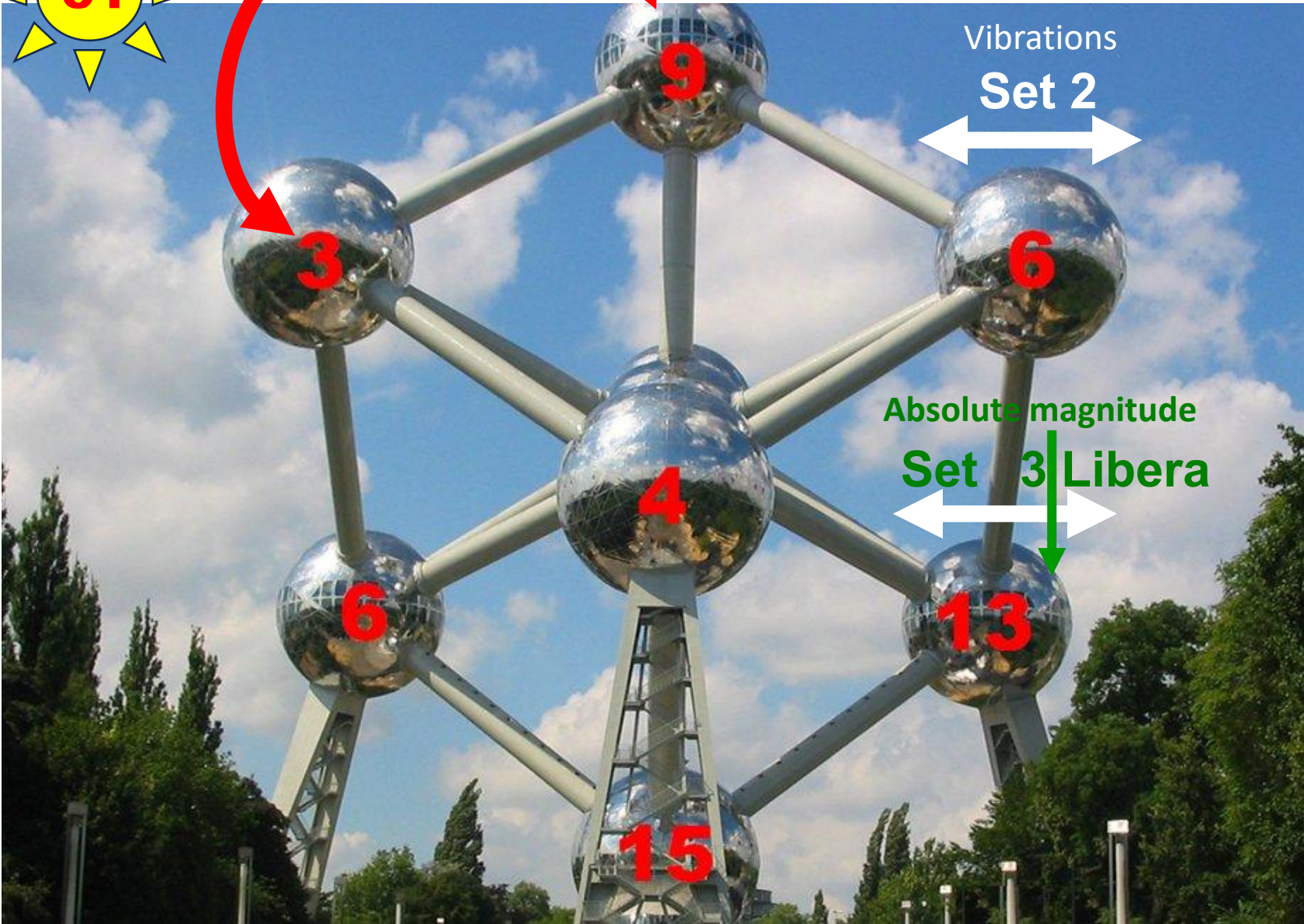
Set 2





Set 1

Equilibrium positions



Vibrations

Set 2

Absolute magnitude

Set 3 Libera

The only input parameter is Incoming Solar

Earth Energy Imbalance (EEI) = 0.54 ± 0.3

LWCRE

1

26.682

N positions are exact

Stephens et al. (2023, BAMS):

"the surface energy balance relation $R_n = LE + H$ "

Stephens (1992):

$R_n = OLR/2$ (clear-sky)

Eq. (3):

$R_n = (OLR - LWCRE) / 2$ (all-sky)

Equations are exact

Incoming Solar
 340.2 ± 0.1

Reflected Solar
 100.2 ± 2.4

Outgoing LW
 239.5 ± 2.4

0.00

340.2
51/4

0.14

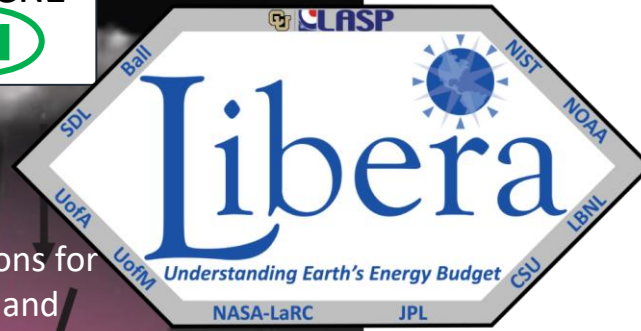
100.06
15/4

-0.64

240.14
36/4

Eq. (3) Sensible heat + Evaporation = (Outgoing LW - LWCRE)/2
 25.4 + 81.1 = (239.5 - 26.68)/2 + **0.1**

Eq. (4) Absorbed SW + All-sky emission = 2 × Outgoing LW + LWCRE
 160.7 + 345.1 = 2 × 239.5 + 26.68 + **0.1**



Precipitation
 81.1 ± 6.1

186.78 **7**

-1.28

26.68 **1**

80.05 **3**

1.05

Integer positions for Sensible heat and Evaporation separately

-2.78

Surface SW
 184.0 ± 5.6

Sensible heat
 25.4 ± 9.4

Evaporation
 81.1 ± 6.1

346.87 **13**

0.61

Absorbed SW
 160.7 ± 5.3

Surface Reflection
 23.3 ± 2.0

-3.38

+0.46

Surface emission
 400.7 ± 4.8

All-sky emission
 345.1 ± 5.7

160.09 **6**

26.68 **1**

400.24 **15**

-1.77

This is our recent understanding of Earth's Energy Budget

Stephens et al. (2023, BAMS)

30 Years of GEWEX



The only input parameter is Incoming Solar

Earth Energy Imbalance (EEI) = 0.54 ± 0.3

LWCRE

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26.682

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Equations are exact

Incoming Solar
 340.2 ± 0.1

0.00

340.2
51/4

Reflected Solar
 100.2 ± 2.4

0.14

100.06
15/4

Outgoing LW
 239.5 ± 2.4

-0.64

240.14
36/4

Eq. (3) Sensible heat + Evaporation = (Outgoing LW - LWCRE)/2
 25.4 + 81.1 = (239.5 - 26.68)/2 + **0.1**

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 160.7 + 345.1 = 2 × 239.5 + 26.68 + **0.1**

Precipitation
 81.1 ± 6.1

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80.05 **3**

1.05

Sensible heat
 25.4 ± 9.4

Evaporation
 81.1 ± 6.1

Integer positions for Sensible heat and Evaporation separately

Absorbed SW
 160.7 ± 5.3

0.61

160.09 **6**

Surface Reflection
 23.3 ± 2.1

-3.38

26.68 **1**

+0.46

Surface emission
 400.7 ± 4.8

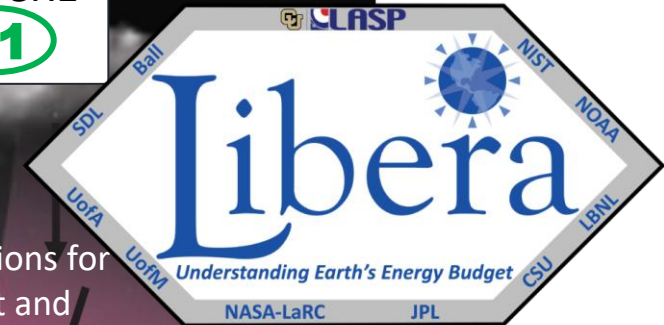
400.24 **15**

-1.77

All-sky emission
 345.1 ± 5.7

346.87 **13**

All-sky emission
 345.1 ± 5.7



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Equations are exact

Incoming Solar
 340.2 ± 0.1

0.00

340.2
51/4

Reflected Solar
 100.2 ± 2.4

0.14

100.06
15/4

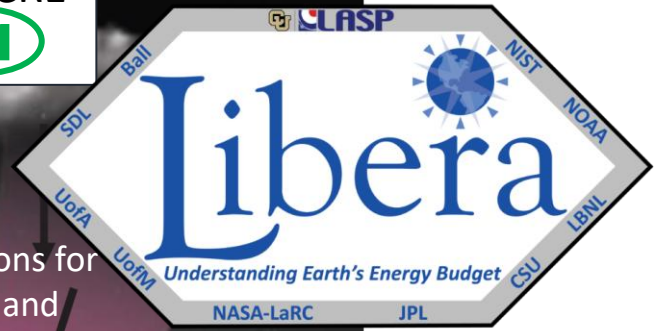
Outgoing LW
 239.5 ± 2.4

-0.64

240.14
36/4

Eq. (3) Sensible heat + Evaporation = (Outgoing LW - LWCRE)/2
 25.4 + 81.1 = (239.5 - 26.68)/2 + **0.1**

Eq. (4) Absorbed SW + All-sky emission = 2 × Outgoing LW + LWCRE
 160.7 + 345.1 = 2 × 239.5 + 26.68 + **0.1**



Precipitation
 81.1 ± 6.1

186.78 **7**
Surface SW
 184.0 ± 5.6

-2.78

-1.28

26.68 **1**
Sensible heat
 25.4 ± 9.4

80.05 **3**
Evaporation
 81.1 ± 6.1

1.05

Integer positions for Sensible heat and Evaporation separately

Surface Reflection
 23.3 ± 2.1

-3.38

Surface emission
 400.7 ± 4.8

+0.46

400.24 **15**

346.87 **13**

All-sky emission
 345.1 ± 5.7

-1.77

0.61

Absorbed SW
 160.7 ± 5.3

160.09 **6**

26.68 **1**

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30 Years of GEWEX



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LWCRE
1
26.682

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51/4

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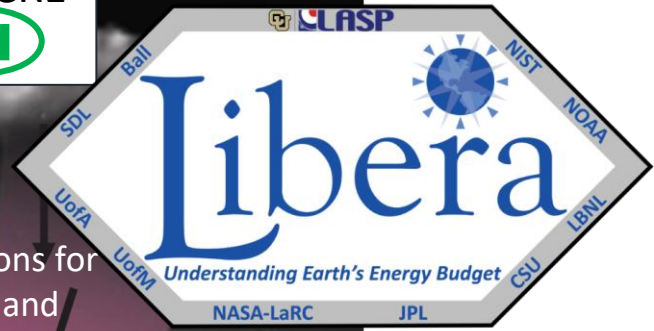
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Integer positions for Sensible heat and Evaporation separately

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160.09 **6**

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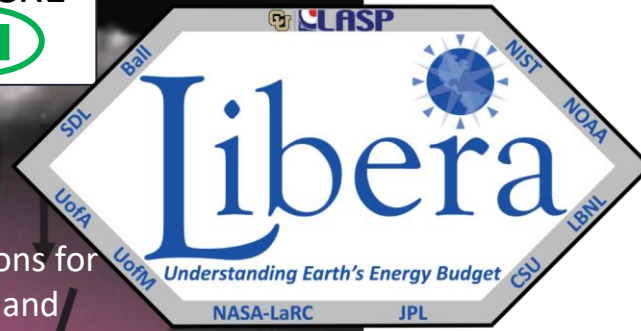
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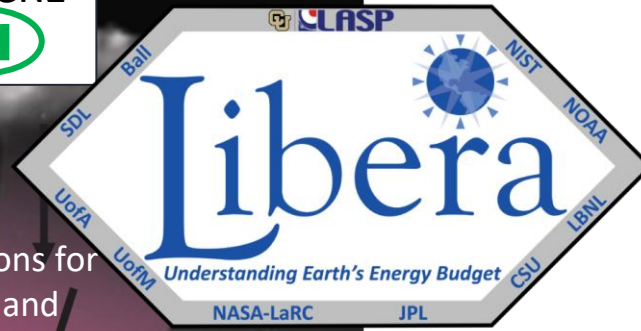
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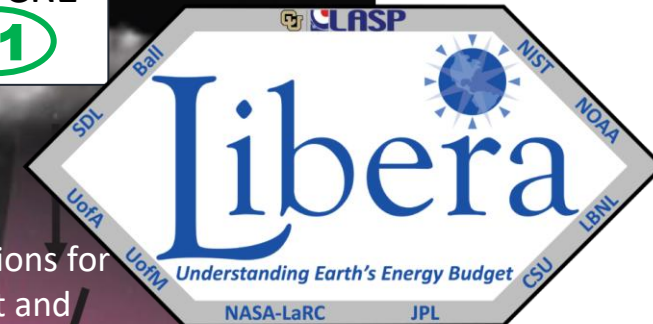
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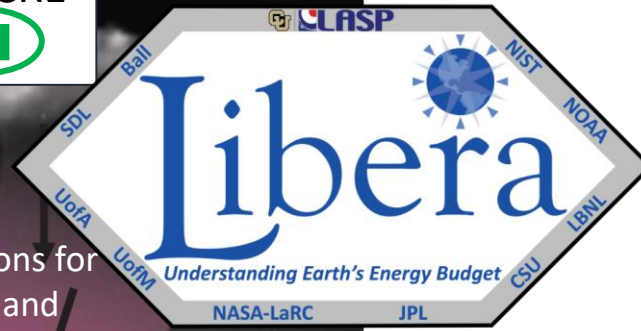
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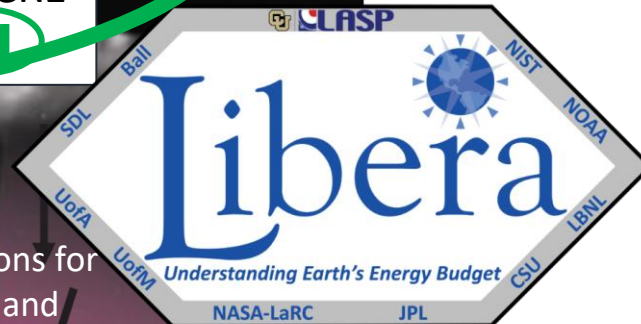
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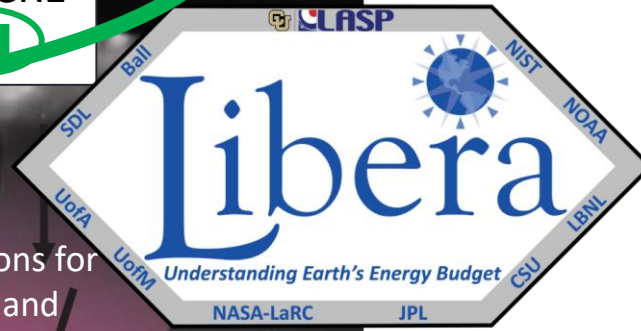
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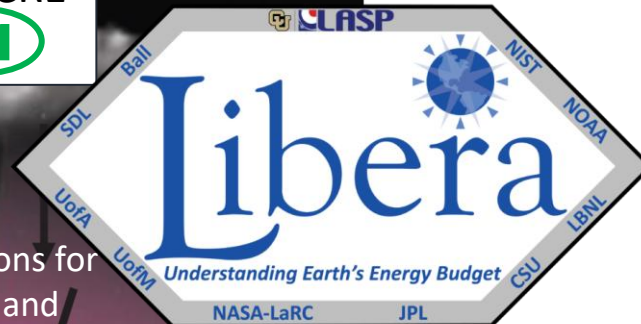
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Summary: 30 Years of CERES Wielicki et al. (1996) (BAMS)

CERES Data Products

Set 1

Stephens et al. (1994) =>

$$R_N = \sigma T_S^4 - \sigma T_0^4 = \text{CONV} = \frac{F_\infty}{2} \quad \text{Eq. (1)}$$

Inamdar and Ramanathan (1994) =>

$$G_a = \sigma T(\tau^*)^4 - f_0 = \text{CONV} = \sigma T_g^4 - \sigma T(\tau^*)^4 = f_0/2 \quad \text{Eq. (2)}$$

$$\begin{aligned} \text{Eq. (1) \& Eq. (2) \Rightarrow } & g_a(\text{clear}) = 1/3 \\ \text{All-sky extension} & g_a(\text{all}) = 2/5 \end{aligned}$$

$$\begin{aligned} \text{Solar Extension: TSI} &= \mathbf{51} \\ \Rightarrow \text{LWCRE} &= \mathbf{1} \end{aligned}$$

$$\begin{aligned} g_a(\text{clear}) &= \mathbf{5/15}, g_a(\text{all}) = \mathbf{6/15} \\ \alpha_p &= \mathbf{15/51} = 0.294 \end{aligned}$$

$$\begin{aligned} \text{EEI} &= \Delta\text{ASR} - \Delta\text{OLR} \\ \Delta F &= \text{Set 2} - \text{Set 1} \end{aligned}$$

Set 2

EBAF Edition 4.2.1 V3 (01/2001 — 12/2025)

Ramanathan and Inamdar (2006): $g_a = 1/3$

$$\begin{aligned} g_a(\text{clear}) &= 0.3333 \\ g_a(\text{all}) &= 0.397 \\ \alpha_p &= 0.291 \end{aligned}$$

$$\begin{aligned} \text{ISR} &= 340.22 \text{ Wm}^{-2} \\ w_g = 4.0034 \Rightarrow \text{TSI} &= 1362.04 \text{ Wm}^{-2} \end{aligned}$$

$$\mathbf{1} = 26.684 \text{ Wm}^{-2}$$

$$\text{EEI} = (241.38 - 240.15) - (240.48 - 240.15) = 0.90 \text{ Wm}^{-2}$$

Deviation for each flux component = Observed – Equilibrium